

Pitz-Daily Turbulence Case

Jonathan Russell

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Pitz-Daily Problem

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1) Description of the case

The goal of this simulation is to replicate experiment performed in 1983 by Robert W Pitz and John W Daily in which they aimed to assess the effect of combustion on the mean flowfield properties such as mixing layer growth, entrainment rate, and reattachment length. The turbulent mixing layer formed at the rearward facing step after combustion will be what is simulated and the data will be gathered in a similar fashion.

2) Hypothesis

Using the turbulent solvers made available in the open source software OpenFOAM, the experimentally gathered results from Pitz and Daily will be recreated in a simulation. The simulation consists of

- Incompressible flow
- Turbulent flow
- Bidimensional flow
- Viscous flow
- Steady flow

3) Physics of the problem

The simulation will occur in a two-dimensional mesh consisting of a short inlet, a backward facing step, and a converging nozzle as the outlet as shown below.

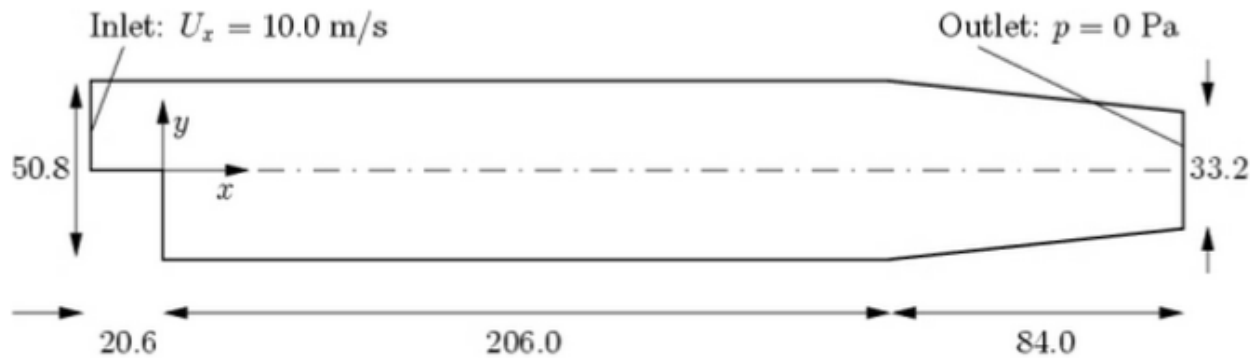


Figure 1: Representation of the model to be used (dimensions in mm)

The governing equations for the problem are as follows:

Mass continuity for incompressible flow

$$\nabla \cdot \mathbf{U} = 0$$

Steady flow momentum equation

$$\nabla \cdot (\mathbf{U}\mathbf{U}) + \nabla \cdot \mathbf{R} = -\nabla p$$

Where p is the kinematic pressure, and \mathbf{R} is the viscous stress term with an effective kinematic viscosity calculated from the transport and turbulence models.

Initial Conditions

- $U = 0$ m/s
- $p = 0$ Pa

Boundary Conditions

- $U_{\text{inlet}} = (10,0,0)$ m/s
- $p_{\text{outlet}} = 0$ Pa

Transport Properties

- kinematic viscosity = $14.0 \mu\text{m}^2/\text{s}$

Turbulence Model

- k-epsilon solver
- Coefficients
 - $C_\mu = 0.09$, $C_1 = 1.44$, $C_2 = 1.92$, $\alpha_k = 1$, $\alpha_{\text{epsilon}} = 0.76$

Solver

- pisoFoam, Large Eddy Simulation



Figure 2: Image of the initial condition (notice the slight increased velocity on the left)

4) Pre-processing

Directories	Constant	0	System
Sub-directories	transportProperties, turbulenceProperties, polyMesh	U, p, nut, nuTilda, k	blockMeshDict, fvSchemes, fvSolution

This is the file structure in which the simulation will be created in. The constant folder sets up the values for coefficients that will be used in the equations the solver uses, the 0 folder contains the initial/boundary conditions, and the system folder has the configuration files for how the mesh is made and how the solver will be executed. The preprocessing involves establishing proper settings for these files based on what scenario is being run. In this case, the values will be chosen to most closely match those given by the Pitz and Daily paper. As well, the data gathering will be performed in a way comparable to the results gathered from the paper to allow for good comparisons.

4a) Mesh Generation

The following code is the blockMeshDict file.

```

1 /*-----*-- C++ -*-----*/
2 |=====|
3 | \ \ / / F i e l d | OpenFOAM: The Open Source CFD Toolbox
4 | \ \ / / O p e r a t i o n | Version: 4.1
5 | \ \ / / A n d | Web: www.OpenFOAM.org
6 | \ \ / / M a n i p u l a t i o n |
7 /*-----*--*/
8 FoamFile
9 {
10     version      2.0;
11     format        ascii;
12     class         dictionary;
13     object        blockMeshDict;
14 }
15 // ***** //
16
17 convertToMeters 0.001;
18
19 vertices
20 (
21     (-20.6 0 -0.5)
22     (-20.6 3 -0.5)
23     (-20.6 12.7 -0.5)
24     (-20.6 25.4 -0.5)
25     (0 -25.4 -0.5)
26     (0 -5 -0.5)
27     (0 0 -0.5)
28     (0 3 -0.5)
29     (0 12.7 -0.5)
30     (0 25.4 -0.5)
31     (206 -25.4 -0.5)
32     (206 -8.5 -0.5)
33     (206 0 -0.5)
34     (206 6.5 -0.5)
35     (206 17 -0.5)
36     (206 25.4 -0.5)
37     (290 -16.6 -0.5)
38     (290 -6.3 -0.5)
39     (290 0 -0.5)
40     (290 4.5 -0.5)
41     (290 11 -0.5)
42     (290 16.6 -0.5)
43     (-20.6 0 0.5)
44     (-20.6 3 0.5)
45     (-20.6 12.7 0.5)
46     (-20.6 25.4 0.5)
47     (0 -25.4 0.5)
48     (0 -5 0.5)
49     (0 0 0.5)
50     (0 3 0.5)
51     (0 12.7 0.5)
52     (0 25.4 0.5)

```

```

53     (206 -25.4 0.5)
54     (206 -8.5 0.5)
55     (206 0 0.5)
56     (206 6.5 0.5)
57     (206 17 0.5)
58     (206 25.4 0.5)
59     (290 -16.6 0.5)
60     (290 -6.3 0.5)
61     (290 0 0.5)
62     (290 4.5 0.5)
63     (290 11 0.5)
64     (290 16.6 0.5)
65 );
66
67 blocks
68 (
69     hex (0 6 7 1 22 28 29 23) (18 7 1) simpleGrading (0.5 1.8 1)
70     hex (1 7 8 2 23 29 30 24) (18 10 1) simpleGrading (0.5 4 1)
71     hex (2 8 9 3 24 30 31 25) (18 13 1) simpleGrading (0.5 0.25 1)
72     hex (4 10 11 5 26 32 33 27) (180 18 1) simpleGrading (4 1 1)
73     hex (5 11 12 6 27 33 34 28) (180 9 1) edgeGrading (4 4 4 4 0.5 1 1 0.5 1 1 1 1)
74     hex (6 12 13 7 28 34 35 29) (180 7 1) edgeGrading (4 4 4 4 1.8 1 1 1.8 1 1 1 1)
75     hex (7 13 14 8 29 35 36 30) (180 10 1) edgeGrading (4 4 4 4 4 1 1 4 1 1 1 1)
76     hex (8 14 15 9 30 36 37 31) (180 13 1) simpleGrading (4 0.25 1)
77     hex (10 16 17 11 32 38 39 33) (25 18 1) simpleGrading (2.5 1 1)
78     hex (11 17 18 12 33 39 40 34) (25 9 1) simpleGrading (2.5 1 1)
79     hex (12 18 19 13 34 40 41 35) (25 7 1) simpleGrading (2.5 1 1)
80     hex (13 19 20 14 35 41 42 36) (25 10 1) simpleGrading (2.5 1 1)
81     hex (14 20 21 15 36 42 43 37) (25 13 1) simpleGrading (2.5 0.25 1)
82 );
83
84 edges
85 (
86 );
87
88 boundary
89 (
90     inlet
91     {
92         type patch;
93         faces
94         (
95             (0 22 23 1)
96             (1 23 24 2)
97             (2 24 25 3)
98         );
99     }
100     outlet

```

```

101     {
102         type patch;
103         faces
104         (
105             (16 17 39 38)
106             (17 18 40 39)
107             (18 19 41 40)
108             (19 20 42 41)
109             (20 21 43 42)
110         );
111     }
112     upperWall
113     {
114         type wall;
115         faces
116         (
117             (3 25 31 9)
118             (9 31 37 15)
119             (15 37 43 21)
120         );
121     }
122     lowerWall
123     {
124         type wall;
125         faces
126         (
127             (0 6 28 22)
128             (6 5 27 28)
129             (5 4 26 27)
130             (4 10 32 26)
131             (10 16 38 32)
132         );
133     }
134     frontAndBack
135     {
136         type empty;
137         faces
138         (
139             (22 28 29 23)
140             (23 29 30 24)
141             (24 30 31 25)
142             (26 32 33 27)
143             (27 33 34 28)
144             (28 34 35 29)
145             (29 35 36 30)
146             (30 36 37 31)
147             (32 38 39 33)
148             (33 39 40 34)
149             (34 40 41 35)
150             (35 41 42 36)
151             (36 42 43 37)

```

```

152         (0 1 7 6)
153         (1 2 8 7)
154         (2 3 9 8)
155         (4 5 11 10)
156         (5 6 12 11)
157         (6 7 13 12)
158         (7 8 14 13)
159         (8 9 15 14)
160         (10 11 17 16)
161         (11 12 18 17)
162         (12 13 19 18)
163         (13 14 20 19)
164         (14 15 21 20)
165     );
166 }
167 );
168
169 mergePatchPairs
170 (
171 );
172
173 // *****

```

In OpenFOAM the mesh is required to be three-dimensional which is why under the vertices section all the values contain three entries. This will be ignored for the most part and the z dimension will be very small and the mesh will be only one unit in that direction.

To start the code, since the values given have been in millimeters, the `convertToMeters` function is called so all the millimeter positions will be properly used as meters in calculations.

The vertices section creates points in space at the given coordinates, anywhere there is a discontinuity or a new definition in the initial/boundary conditions a vertex will have to be placed.

The blocks code the creates the divisions used in the mesh. In this case, locations away from the edges all have a uniform grading, meaning the mesh is equally divided into (x y z) number of divisions. As can be seen in the code above, the mesh is more defined in areas of interest such as edges and the backward facing step.

The boundary section establishes which vertices are the outer boundaries of the wall, and if there are certain boundary conditions that will be applied to them (i.e. inlet, outlet, interface).

4b) Initial/Boundary Conditions

As stated earlier the parameters in these next files were made to be as similar to the Pitz-Dialy case as possible

Initial pressure file

```
1 /*----- C++ -----*/
2 |=====|
3 | \ \ \ / | F ield | OpenFOAM: The Open Source CFD Toolbox
4 | \ \ \ / | O peration | Version: 4.1
5 | \ \ \ / | A nd | Web: www.OpenFOAM.org
6 | \ \ \ / | M anipulation |
7 /*-----*/
8 FoamFile
9 {
10     version      2.0;
11     format        ascii;
12     class         volScalarField;
13     object        p;
14 }
15 // *****
16
17 dimensions      [0 2 -2 0 0 0];
18
19 internalField    uniform 0;
20
21 boundaryField
22 {
23     inlet
24     {
25         type      zeroGradient;
26     }
27
28     outlet
29     {
30         type      fixedValue;
31         value      uniform 0;
32     }
33
34     upperWall
35     {
36         type      zeroGradient;
37     }
38
39     lowerWall
40     {
41         type      zeroGradient;
42     }
43
44     frontAndBack
45     {
46         type      empty;
47     }
48 }
49
50 // ***** //
```

This is the Velocity initial condition file

```
3 | \\ / F i e l d | OpenFOAM: The Open Source CFD Toolbox |
4 | \\ / O p e r a t i o n | Version: 4.1 |
5 | \\ / A n d | Web: www.OpenFOAM.org |
6 | \\ / M a n i p u l a t i o n | |
7 | *-----* |
8 FoamFile
9 {
10     version      2.0;
11     format        ascii;
12     class         volVectorField;
13     object        U;
14 }
15 // *****
16
17 dimensions      [0 1 -1 0 0 0 0];
18
19 internalField    uniform (0 0 0);
20
21 boundaryField
22 {
23     inlet
24     {
25         type       turbulentInlet;
26         referenceField uniform (10 0 0);
27         fluctuationScale (0.02 0.01 0.01);
28         value       uniform (10 0 0);
29     }
30
31     outlet
32     {
33         type       inletOutlet;
34         inletValue  uniform (0 0 0);
35         value       uniform (0 0 0);
36     }
37
38     upperWall
39     {
40         type       noSlip;
41     }
42
43     lowerWall
44     {
45         type       noSlip;
46     }
47
48     frontAndBack
49     {
50         type       empty;
51     }
52 }
53
54 // *****
```

The inlet section was made to act as if it were the turbulent inlet velocity from the paper. It was treated as if it were a uniform velocity from top to bottom. The outlet is outputting to the atmosphere so it is initially static.

This is the initial turbulent kinetic energy (k) file.

```
3 | \\ / F i e l d | OpenFOAM: The Open Source CFD Toolbox |
4 | \\ / O p e r a t i o n | Version: 4.1 |
5 | \\ / A n d | Web: www.OpenFOAM.org |
6 | \\ / M a n i p u l a t i o n | |
7 | *-----* |
8 FoamFile
9 {
10     version      2.0;
11     format        ascii;
12     class         volScalarField;
13     object        k;
14 }
15 // *****
16
17 dimensions      [0 2 -2 0 0 0 0];
18
19 internalField    uniform 0;
20
21 boundaryField
22 {
23     inlet
24     {
25         type      fixedValue;
26         value      uniform 2e-05;
27     }
28
29     outlet
30     {
31         type      inletOutlet;
32         inletValue uniform 0;
33         value      uniform 0;
34     }
35
36     upperWall
37     {
38         type      fixedValue;
39         value      uniform 0;
40     }
41
42     lowerWall
43     {
44         type      fixedValue;
45         value      uniform 0;
46     }
47
48     frontAndBack
49     {
50         type      empty;
51     }
52 }
53
54 // *****
```

the turbulent kinetic energy was set to be zero except at the inlet where it is assumed to be isotropic and have initially small fluctuations, hence the small value of k.

This is the turbulent viscosity file (note: nuT is used for LES and nuTilda is used for RAS)

```

1 /*-----*- C++ -*-----*/
2 |=====|
3 | \ \ / / F i e l d | OpenFOAM: The Open Source CFD Toolbox
4 | \ \ / / O peration | Version: 4.1
5 | \ \ / / A nd | Web: www.OpenFOAM.org
6 | \ \ / / M anipulation |
7 /*-----*- C++ -*-----*/
8 FoamFile
9 {
10     version      2.0;
11     format        ascii;
12     class         volScalarField;
13     object        nut;
14 }
15 // *****
16
17 dimensions      [0 2 -1 0 0 0 0];
18
19 internalField    uniform 0;
20
21 boundaryField
22 {
23     inlet
24     {
25         type      zeroGradient;
26     }
27
28     outlet
29     {
30         type      zeroGradient;
31     }
32
33     upperWall
34     {
35         type      zeroGradient;
36     }
37
38     lowerWall
39     {
40         type      zeroGradient;
41     }
42
43     frontAndBack
44     {
45         type      empty;
46     }
47 }
48
49 // *****

```

This establishes the viscosity to not be spatially dependent, the value for it will be calculated by the solver using the relationship $\nu T = l * k^{0.5}$

4c) Physical Properties

This file establishes how the turbulence will be modeled by the simulation

```
1 /*----- C++ -----*/
2 |=====|
3 | \ \ / / F i e l d | OpenFOAM: The Open Source CFD Toolbox
4 | \ \ / / O p e r a t i o n | Version: 4.1
5 | \ \ / / A n d | Web: www.OpenFOAM.org
6 | \ \ / / M a n i p u l a t i o n |
7 /*-----*/
8 FoamFile
9 {
10     version      2.0;
11     format        ascii;
12     class         dictionary;
13     location      "constant";
14     object        turbulenceProperties;
15 }
16 // *****
17
18 simulationType LES;
19
20 LES
21 {
22     LESModel      dynamicKEqn;
23
24     turbulence    on;
25
26     printCoeffs   on;
27
28     delta         cubeRootVol;
29
30     dynamicKEqnCoeffs
31     {
32         filter simple;
33     }
34
35     cubeRootVolCoeffs
36     {
37         deltaCoeff 1;
38     }
39
40     PrandtlCoeffs
41     {
42         delta         cubeRootVol;
43         cubeRootVolCoeffs
44         {
45             deltaCoeff 1;
46         }
47
48         smoothCoeffs
49         {
50             delta         cubeRootVol;
51             cubeRootVolCoeffs
```

```

52         {
53             deltaCoeff      1;
54         }
55
56         maxDeltaRatio      1.1;
57     }
58
59     Cdelta      0.158;
60 }
61
62 vanDriestCoeffs
63 {
64     delta      cubeRootVol;
65     cubeRootVolCoeffs
66     {
67         deltaCoeff      1;
68     }
69
70     smoothCoeffs
71     {
72         delta      cubeRootVol;
73         cubeRootVolCoeffs
74         {
75             deltaCoeff      1;
76         }
77
78         maxDeltaRatio      1.1;
79     }
80
81     Aplus      26;
82     Cdelta      0.158;
83 }
84
85 smoothCoeffs
86 {
87     delta      cubeRootVol;
88     cubeRootVolCoeffs
89     {
90         deltaCoeff      1;
91     }
92
93     maxDeltaRatio      1.1;
94 }
95 }
96
97
98 // ***** //

```

In this case Large Eddy Simulation (LES) is used as RAS requires large time steps and this problem is on a very small time scale. Specifically, the dynamic one equation eddy-viscosity model is used.

The values of coefficients and ratios were chosen based on other similar simulations of similar space-time scale.

The solution is using a dynamic subgrid-scale model which computes coefficients dynamically as the simulation occurs, but a drawback of such is that it performs poorly near walls or transitional regimes.

This is the file that defines the values of viscosity for the simulation

```
1 |/*-----*-- C++ --*-----*\
2 |
3 |=====| F ield      | OpenFOAM: The Open Source CFD Toolbox
4 |\\      | O peration | Version: 4.1
5 |\\      | A nd       | Web:      www.OpenFOAM.org
6 |\\      | M anipulation|
7 |*-----*\
8 FoamFile
9 {
10     version      2.0;
11     format        ascii;
12     class         dictionary;
13     location      "constant";
14     object        transportProperties;
15 }
16 // * * * * *
17
18 transportModel  Newtonian;
19
20 nu              [0 2 -1 0 0 0 0] 1e-05;
21
22 // ***** //
```

4d) Control Case

controlDict (probes, uniform something something), fvSchemes, fvSolution

```
1 /*----- C++ -----*/
2 |=====|
3 | \ \ / F i e l d | OpenFOAM: The Open Source CFD Toolbox
4 | \ \ / O p e r a t i o n | Version: 4.1
5 | \ \ / A n d | Web: www.OpenFOAM.org
6 | \ \ / M a n i p u l a t i o n |
7 /*-----*/
8 FoamFile
9 {
10     version      2.0;
11     format        ascii;
12     class          dictionary;
13     location       "system";
14     object         controlDict;
15 }
16 // *****
17
18 application      pisoFoam;
19
20 startFrom        startTime;
21
22 startTime        0;
23
24 stopAt           endTime;
25
26 endTime          0.1;
27
28 deltaT           2e-05;
29
30 writeControl      timeStep;
31
32 writeInterval     10;
33
34 purgeWrite        0;
35
36 writeFormat       ascii;
37
38 writePrecision    6;
39
40 writeCompression  off;
41
42 timeFormat        general;
43
44 timePrecision     6;
45
46 runTimeModifiable true;
47
48 functions
49 {
50     probes
51     {
52         type        probes;
```

```

53     libs          ("libsampling.so");
54     writeControl   timeStep;
55     writeInterval  1;
56
57     fields
58     (
59         p
60     );
61
62     probeLocations
63     (
64         (0.0254 0.0253 0)
65         (0.0508 0.0253 0)
66         (0.0762 0.0253 0)
67         (0.1016 0.0253 0)
68         (0.127 0.0253 0)
69         (0.1524 0.0253 0)
70         (0.1778 0.0253 0)
71     );
72
73 }
74
75 fieldAverage1
76 {
77     type          fieldAverage;
78     libs          ("libfieldFunctionObjects.so");
79     writeControl   writeTime;
80
81     fields
82     (
83         U
84         {
85             mean          on;
86             prime2Mean    on;
87             base          time;
88         }
89
90         p
91         {
92             mean          on;
93             prime2Mean    on;
94             base          time;
95         }
96     );
97 }
98
99 surfaceSampling
100 {

```

```

101 // Sample near-wall velocity
102
103 type surfaces;
104
105 // Where to load it from (if not already in solver)
106 libs ("libsampling.so");
107 writeControl writeTime;
108
109 interpolationScheme cellPoint;
110
111 surfaceFormat vtk;
112
113 // Fields to be sampled
114 fields
115 (
116     U
117 );
118
119 surfaces
120 (
121     nearWall
122     {
123         type patchInternalField;
124         patches ( lowerWall );
125         distance 1E-6;
126         interpolate true;
127         triangulate false;
128     }
129 );
130 }
131
132 #includeFunc scalarTransport
133 }
134
135 // *****

```

This file allows most of the control of the simulation's precision. As per the experiment, the simulation should take about 0.1 seconds. The write interval will determine how many times the data will be recorded throughout the 0.1 seconds, and the precision of the data recorded can also be altered with writeprecision and timeprecision. Choosing a proper deltaT is important, in this case based on the chosen division of spatial parameters, the maximum deltaT is as chosen (2e-05), but if more time temporal resolution is desired this can be decreased, but it comes at a significant simulation time cost.

In the paper, several probes were used to record the data, so instead of comparing the overall data from the simulation, looking at probes placed through the tube on the same axial point will be beneficial. The probes record the data at the defined cell throughout the entire simulation and is output to a file displaying the resulting pressure over time. As well, the fieldaverage method can be used to obtain the average values for velocity along the lowerWall over time. This can be compared to the velocity profiles gathered by Pitz and Daily and it is important because the solver is known to be weaker near the edges, so any validation here would hold strong weight.

This is the fvSchemes file

```
2 | ===== |
3 | \ \ \ \ \ | F i e l d | OpenFOAM: The Open Source CFD Toolbox
4 | \ \ \ \ \ | O p e r a t i o n | Version: 4.1
5 | \ \ \ \ \ | A n d | Web: www.OpenFOAM.org
6 | \ \ \ \ \ | M a n i p u l a t i o n |
7 | *-----* |
8 FoamFile
9 {
10     version      2.0;
11     format        ascii;
12     class         dictionary;
13     location      "system";
14     object        fvSchemes;
15 }
16 // *****
17
18 ddtSchemes
19 {
20     default        backward;
21 }
22
23 gradSchemes
24 {
25     default        Gauss linear;
26 }
27
28 divSchemes
29 {
30     default        none;
31     div(phi,U)      Gauss LUST grad(U);
32     div(phi,k)      Gauss limitedLinear 1;
33     div(phi,s)      bounded Gauss limitedLinear 1;
34     div((nuEff*dev2(T(grad(U))))) Gauss linear;
35 }
36
37 laplacianSchemes
38 {
39     default        Gauss linear corrected;
40 }
41
42 interpolationSchemes
43 {
44     default        linear;
45 }
46
47 snGradSchemes
48 {
49     default        corrected;
50 }
51
52
53 // ***** //
```

The schemes used were chosen based upon other simulations of turbulent incompressible flow.

This is the fvSolution file

```

1  /*-----*-- C++ -*-----*/
2  |=====|
3  | \ \ \ \ \ \ \ \ | F i e l d | OpenFOAM: The Open Source CFD Toolbox
4  | \ \ \ \ \ \ \ \ | O p e r a t i o n | Version: 4.1
5  | \ \ \ \ \ \ \ \ | A n d | Web: www.OpenFOAM.org
6  | \ \ \ \ \ \ \ \ | M a n i p u l a t i o n |
7  |-----*--*/
8  FoamFile
9  {
10     version      2.0;
11     format        ascii;
12     class         dictionary;
13     location      "system";
14     object        fvSolution;
15 }
16 // *****
17
18 solvers
19 {
20     p
21     {
22         solver      GAMG;
23         tolerance    1e-06;
24         relTol       0.1;
25         smoother     GaussSeidel;
26     }
27
28     pFinal
29     {
30         $p;
31         smoother     DICGaussSeidel;
32         tolerance     1e-06;
33         relTol        0;
34     }
35
36     "(U|k|B|nuTilda|s)"
37     {
38         solver      smoothSolver;
39         smoother     GaussSeidel;
40         tolerance     1e-05;
41         relTol        0;
42     }
43 }
44
45 PISO
46 {
47     nCorrectors      2;
48     nNonOrthogonalCorrectors 0;
49 }
50
51
52 // *****

```

For the turbulent solver a tolerance is required for some of the variables mentioned in the initial conditions and some specific to the turbulence calculations, for which 1e-05 is acceptable, though a slightly more tolerance is desired for p, pFinal especially since it has a low impact on computational time unlike U,k,B,nuT and s. The ncorrectors will determine how many times the pressure equation and momentum corrector, increasing this will have a significant computational time cost. The nNonOrthogonalCorrectors is usually set to 0 for steady-state.

5) Running the Case

To run the case, go back into the /\$FOAM_RUN/pitz folder and run

```
blockMesh
```

```
checkMesh
```

```
pisoFoam
```

The checkMesh is just to ensure there are no glaring issues in the definition of the mesh and after running pisoFoam it should take a while (anywhere from 10 minutes to many hours depending on the precision, and space-time scale).

6) Post Processing

Once the simulation is finished the output files from the probes, field averaging and p/U files will be put into folders for the specific times at which they occurred (i.e. the final result will be in pitz/0.1. To view the overall simulation type paraFoam and the paraFoam data viewer will open and create a directory containing the data from the pitz case. To view this click on the pitz.openfoam in the left window and click apply. The initial time should now be shown. In the scroll down menu p, or U can be selected to see how they looked initially (remember pressure was set to be 0 so nothing should be notable about that).

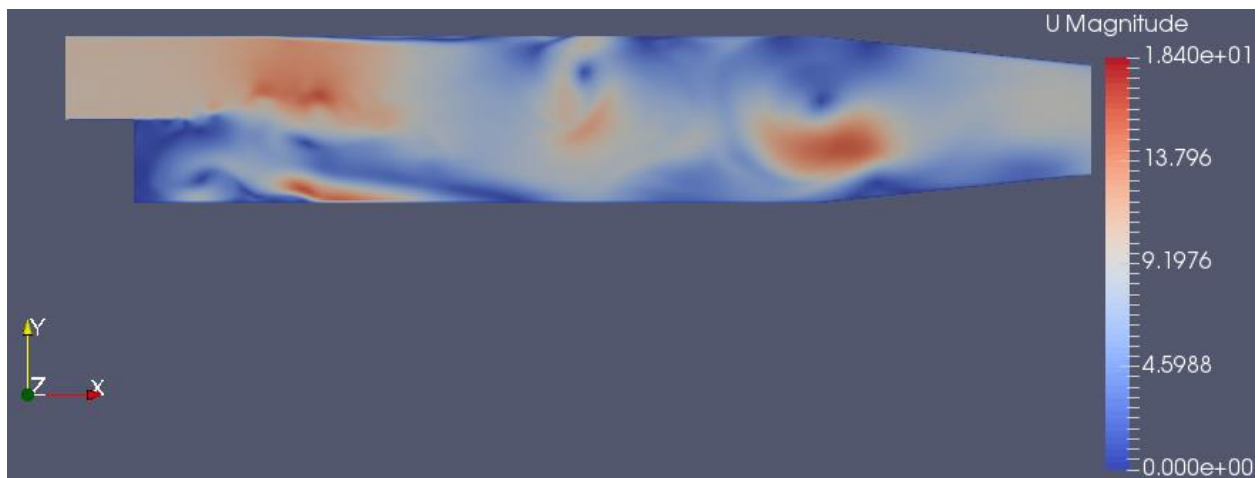


Figure 3: Image of the velocity distribution at the final time

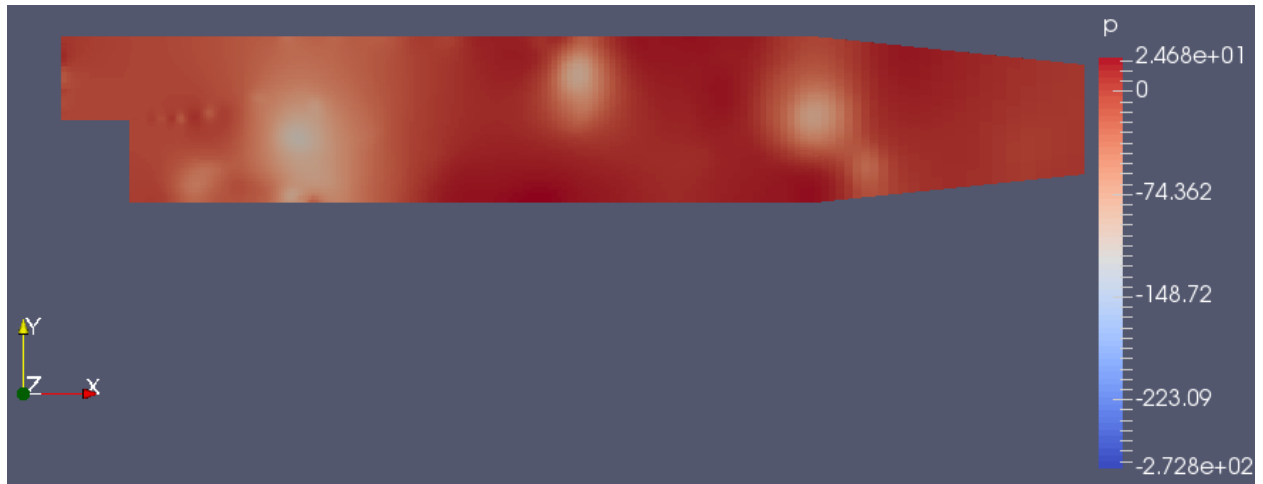


Figure 4: Image of the final pressure distribution