

Wing Geometry Effect on Blade-Vortex Interaction Response Using BEM

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Outline

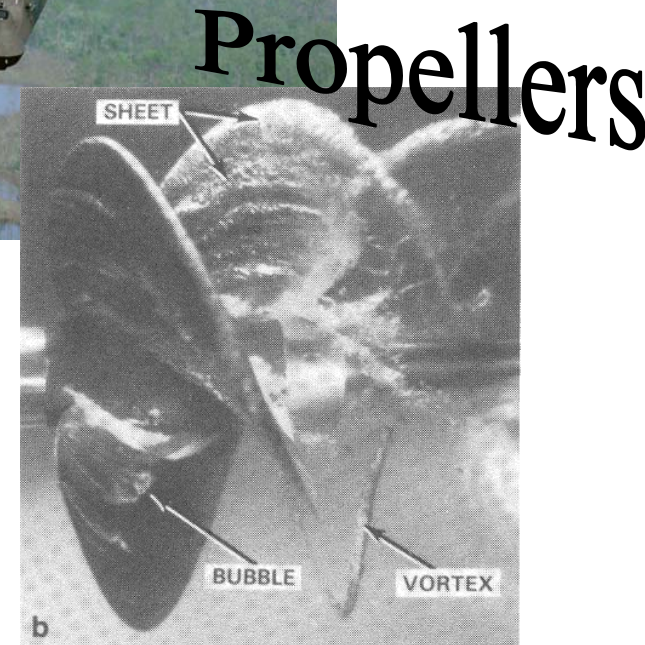
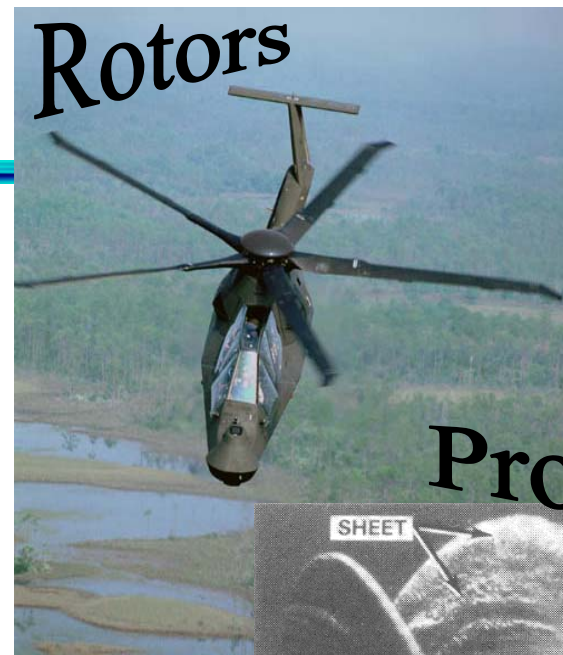
Applications for research

- Rotor BVI problem
- Noise from high-lift wing systems
- Naval propeller shaping

BEM - brief description

Validation of method/classical problems

Wing shape effects



Rotor noise/BVI



On landing rotor/wake interactions --> beating sound
Blade shaping



XV15 landing (tiltrotor)

Airframe noise



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High-lift wing systems
split flaps, slat tracks,
blown flaps



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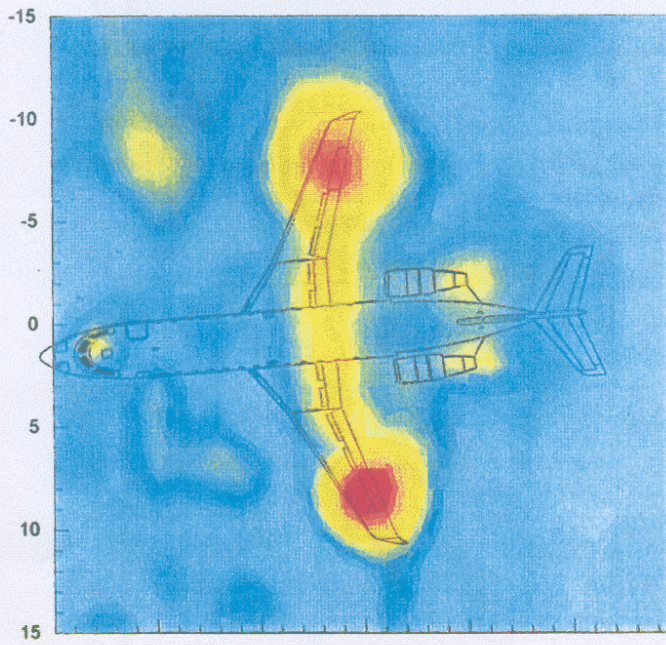
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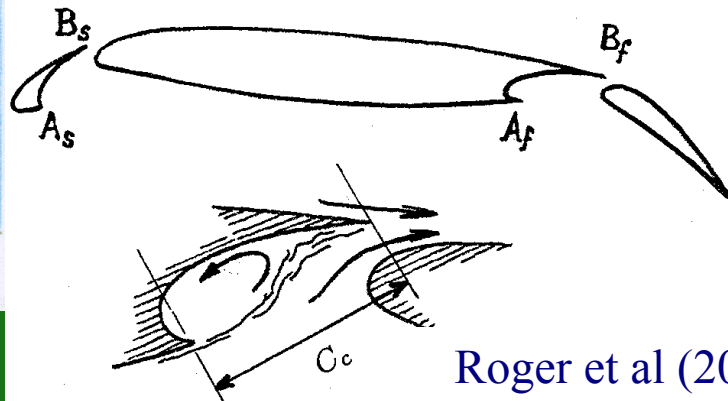
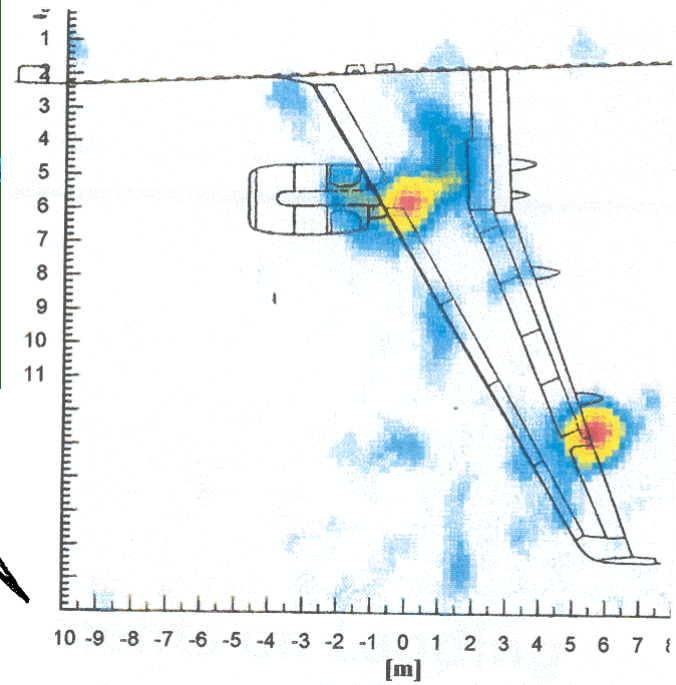
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Wing noise

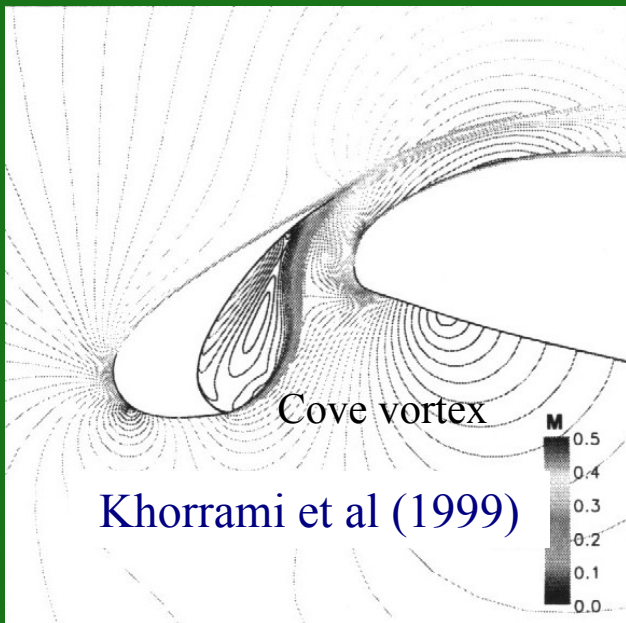


Michel et. al. (1998)

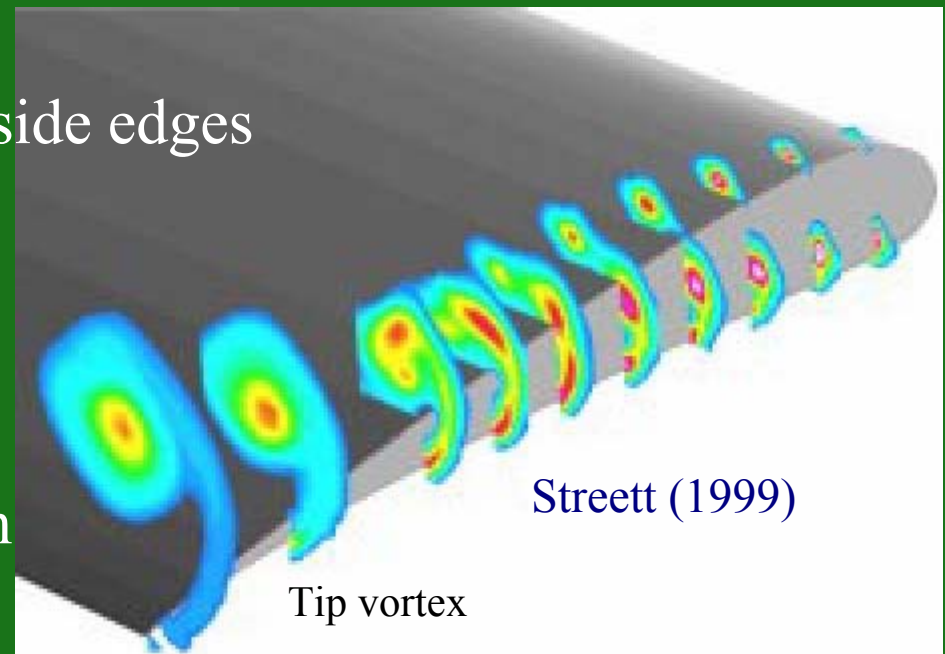


Roger et al (2000)

Gaps



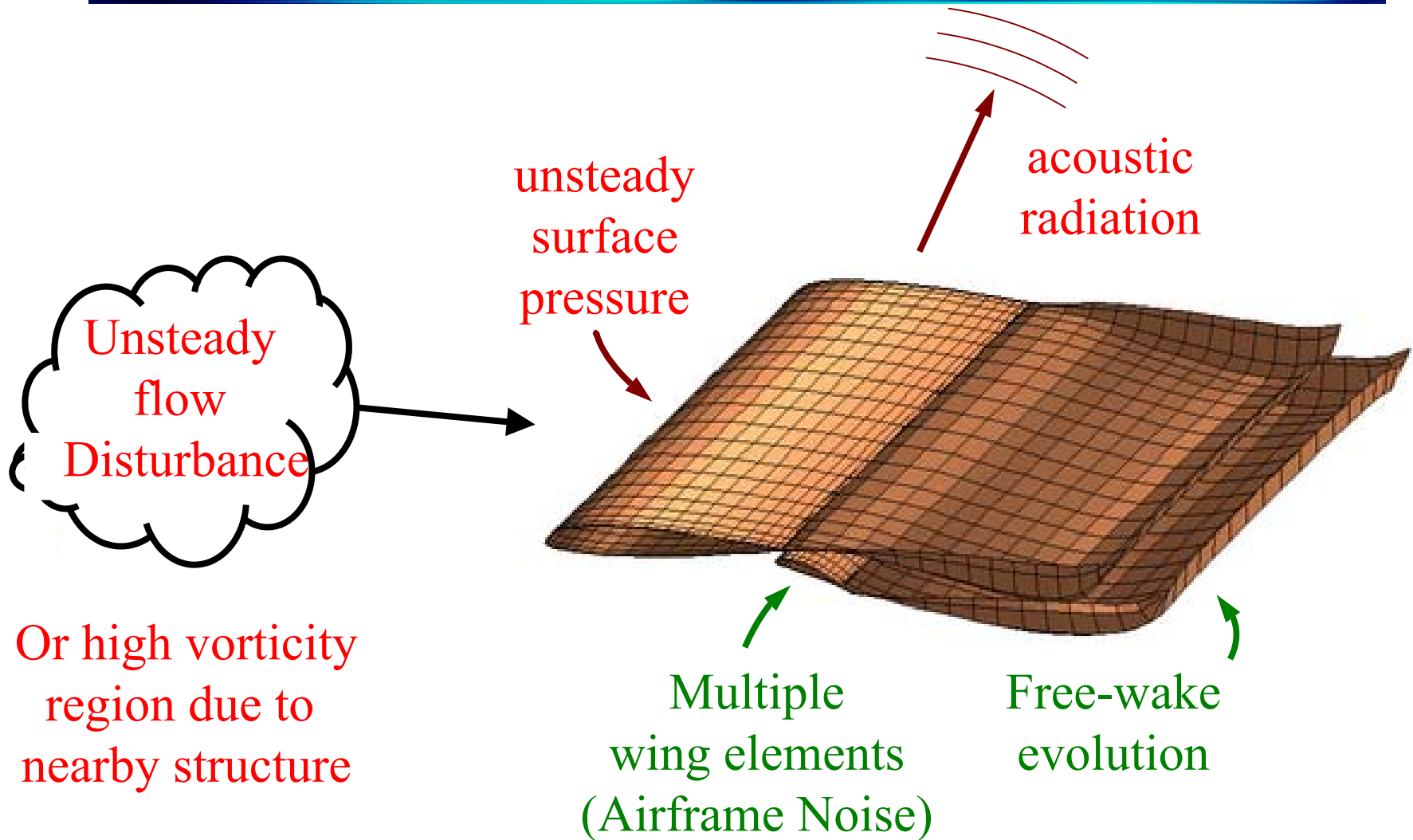
Flap side edges



Regions of high vorticity

Streett (1999)

Underlying Problem

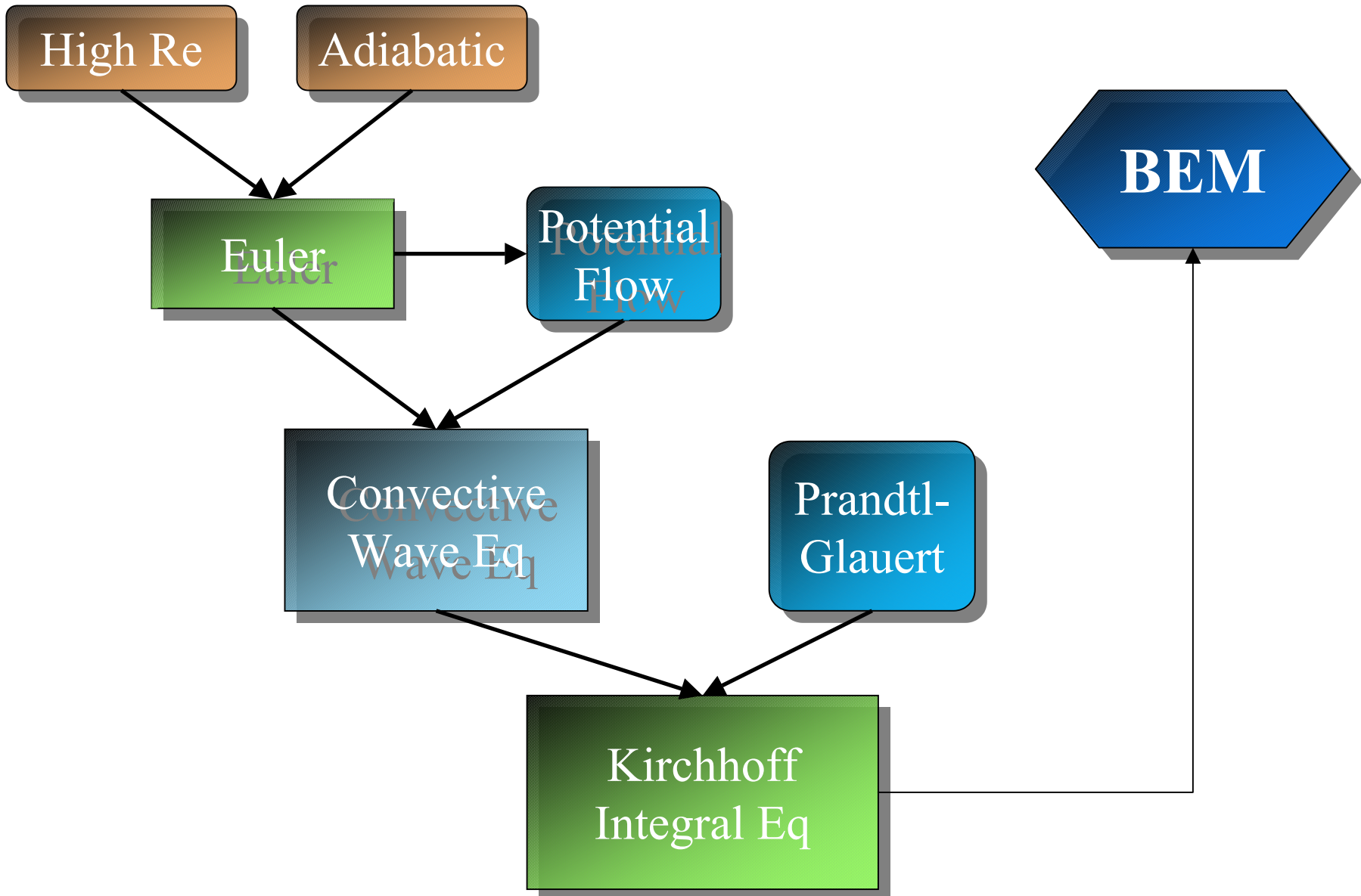


BEM Method

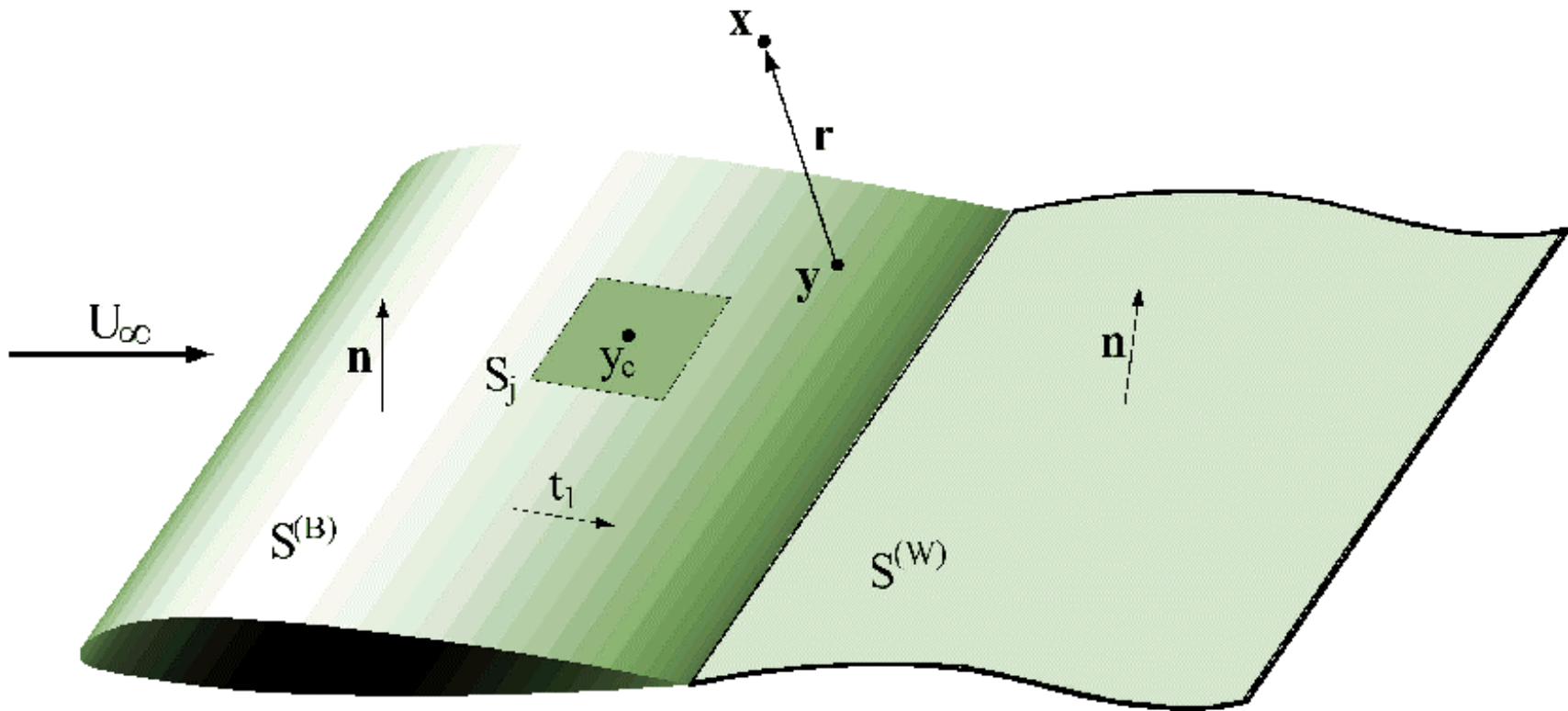
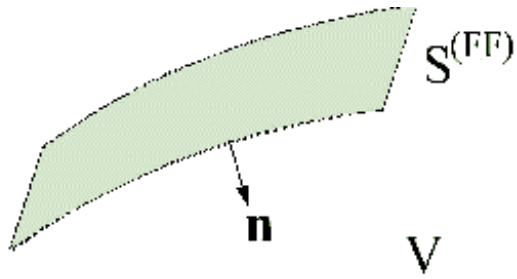
Boundary Element Method (BEM)

- Widely-used for aerodynamics (High Re, attached)
- Past research on:
 - 2D / 3D steady / frequency / time domain
 - Free wake, boundary layers, separation, transonic
- Current Capabilities:
 - 3D Multi-element, Time domain, Compressible
 - Acoustic Evaluation
 - Free wake, Free vortex evolution
 - Accurate **fixed-wake** model using steady **free wake**

Method



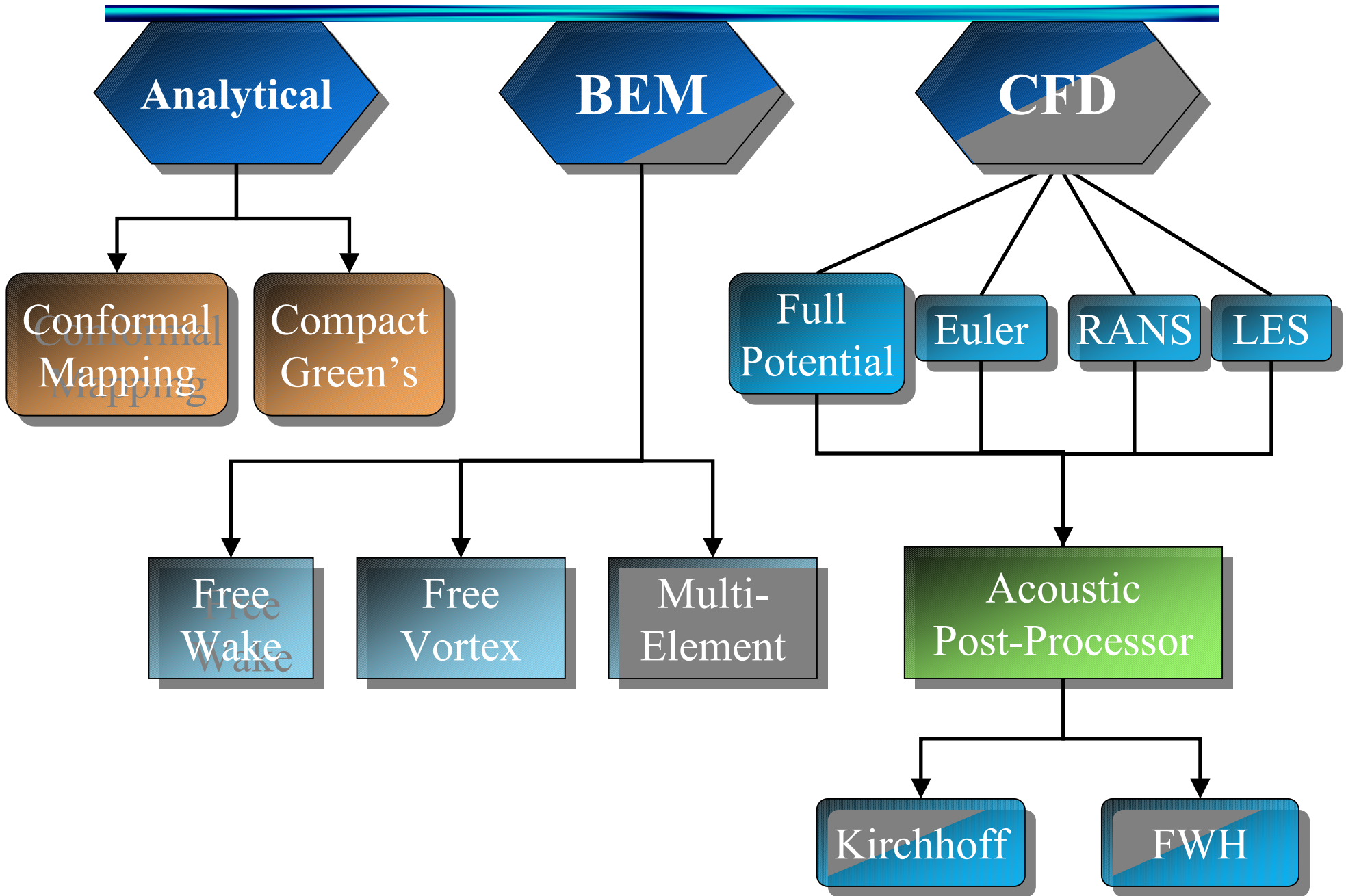
Method



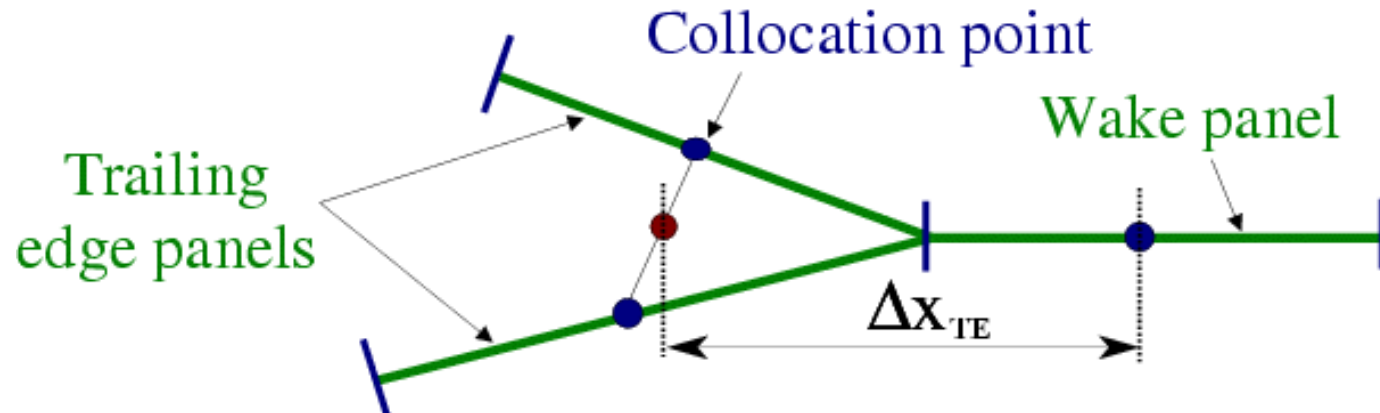
$$\mathbf{v} = \nabla\phi + U_{\infty}\hat{i}$$

$$\phi(\mathbf{x}, t) = \int_S \left[G_S \frac{\partial\phi}{\partial n} + G_D(\mathbf{x}, t|\mathbf{y}, \tau)\phi(\mathbf{y}, \tau) + G_R \frac{\partial\phi}{\partial\tau} \right]_{\tau^*} dS_y$$

Impermeability/know downwash



Trailing Edge Condition



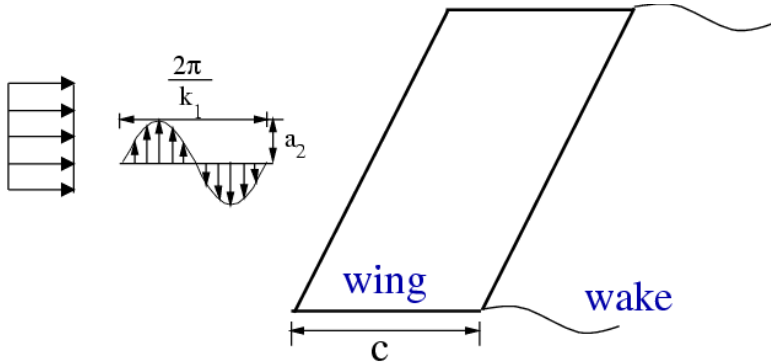
Kutta Condition:

$$\Delta p_{TE} = 0 \quad \longrightarrow \quad \Delta \phi_{TE}^{(B)} = \Delta \phi_{TE}^{(W)}$$

0th order BEM:

$$\Delta \phi_{TE}^{(W)} = \left[\phi_{(TE+)}^{(B)} - \phi_{(TE-)}^{(B)} \right]_{t - \Delta x_{TE} / U_{\infty}}$$

Sears Problem



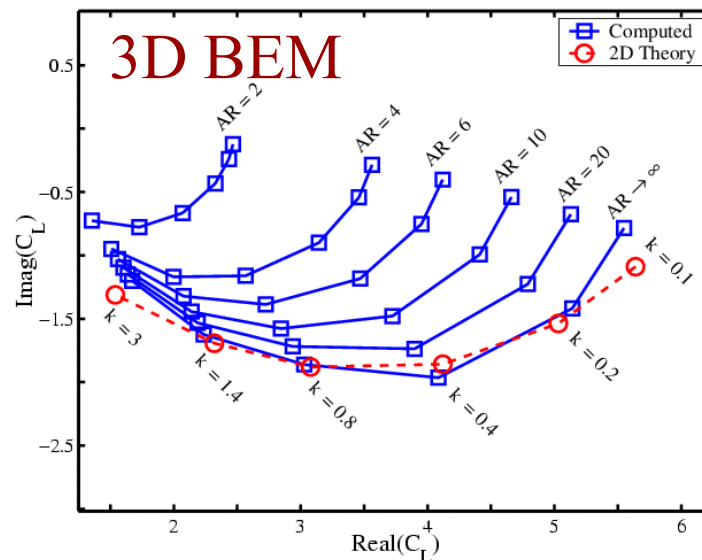
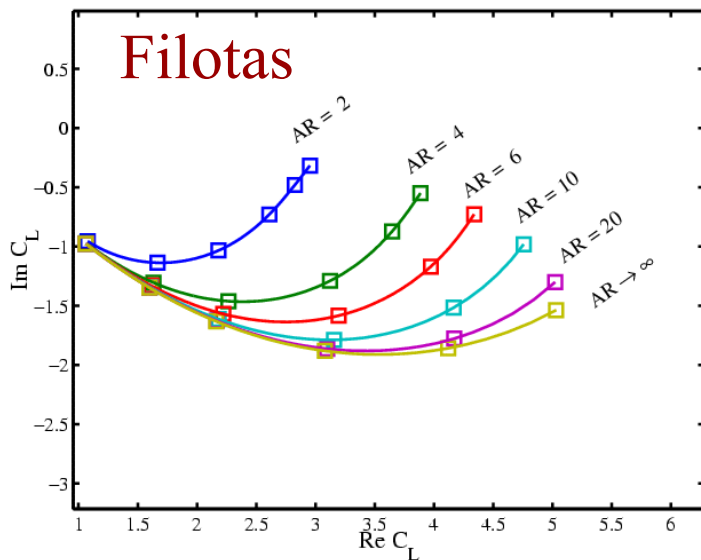
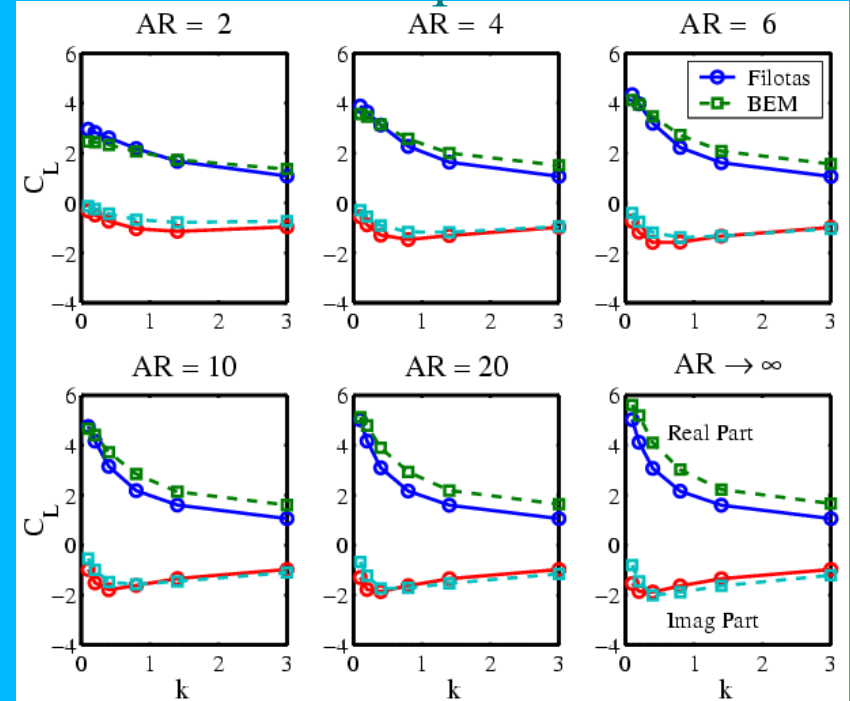
Downwash velocity

$$\mathbf{v}(x_1, x_3, t) = A(k)e^{-ik(t-x_1)}\hat{j}$$

Large aspect ratio, Filotas solution

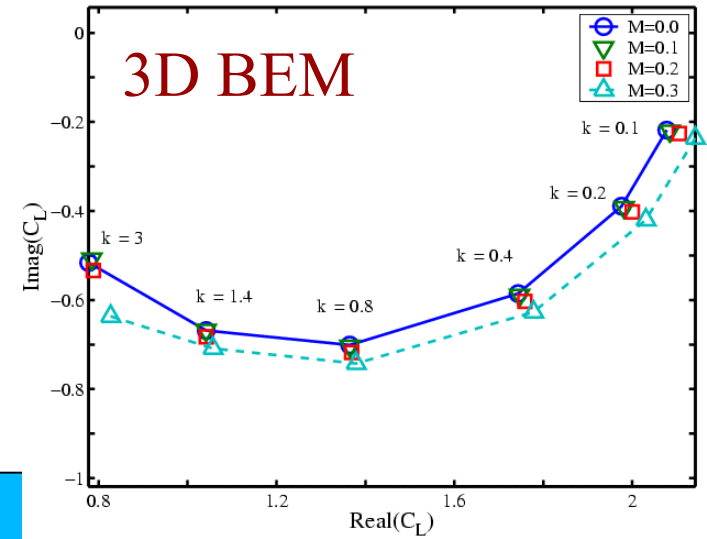
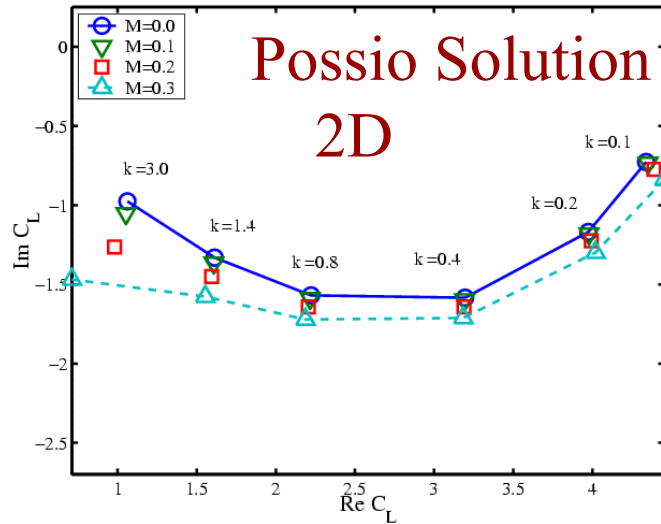
$$C_L = \frac{L}{\frac{1}{2}\rho_\infty U_\infty^2 S_A} = 2\pi A(k)S_B(k, AR)e^{-ikt}$$

Comparison



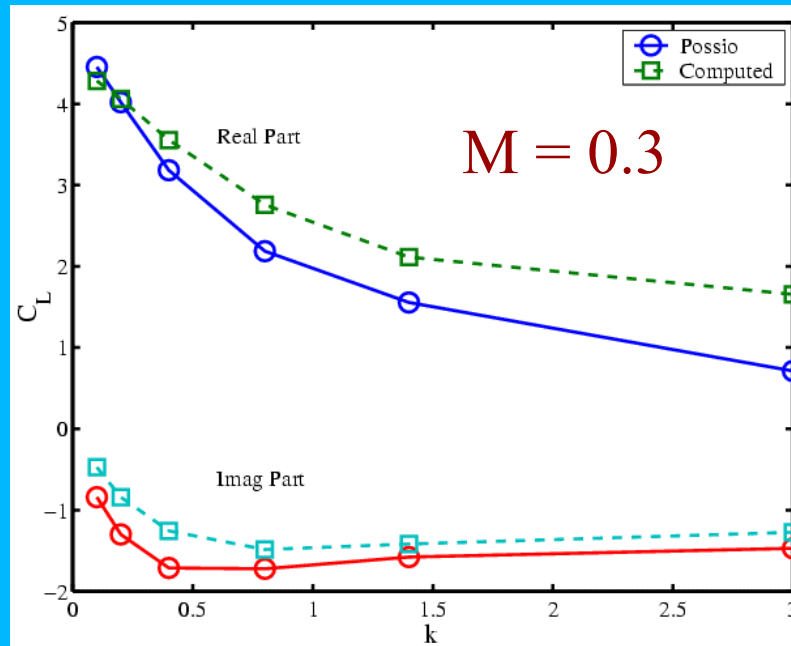
Extrapolation (1/N)
using N=10,12,14

Compressible Problem

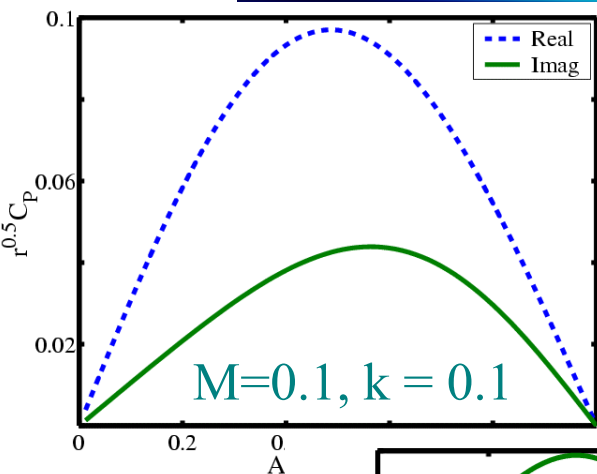


Comparison

Computations
for $AR=6.0$
(Difference due to
3D effects)

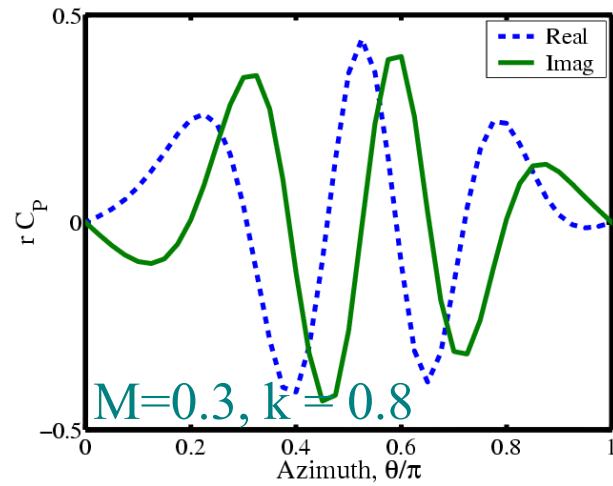
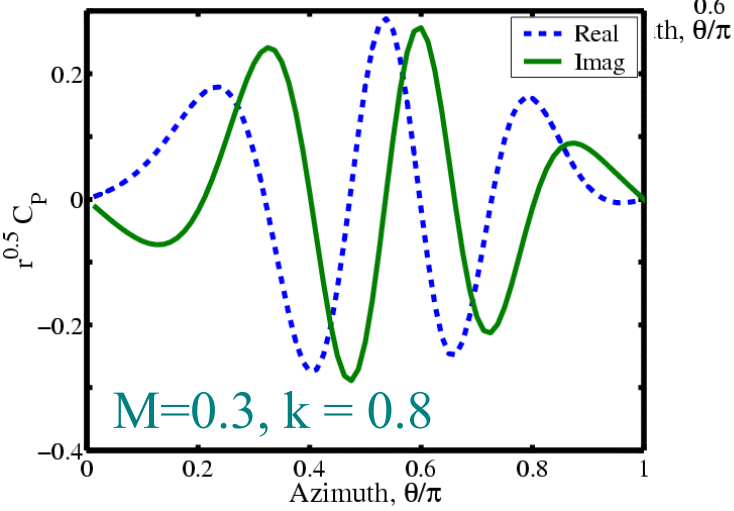
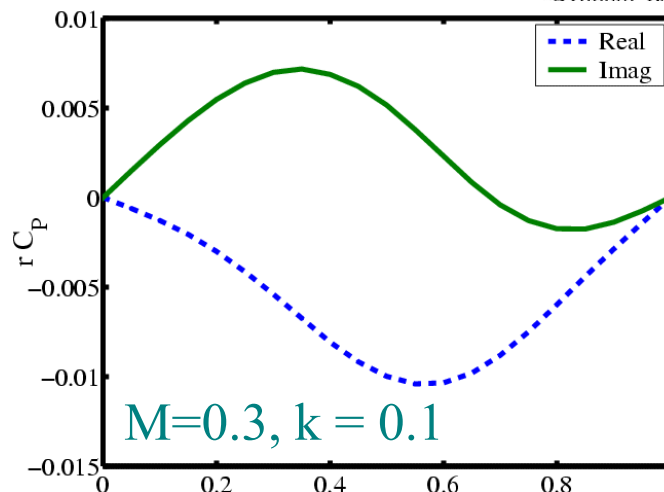
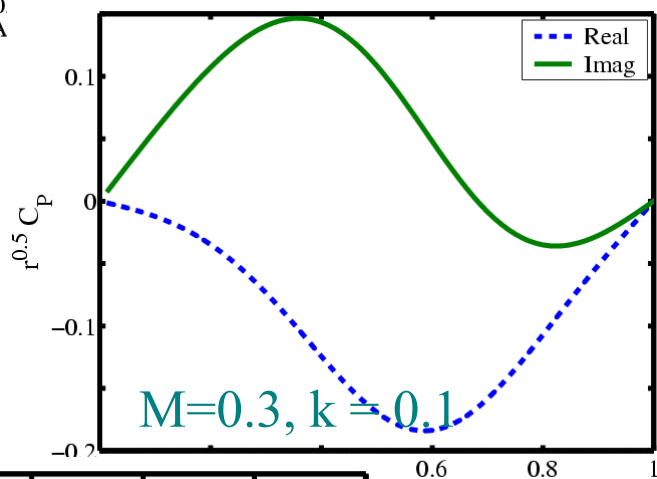
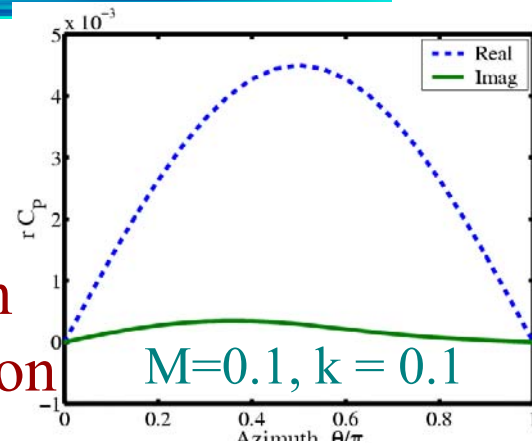


Far-field for Sears

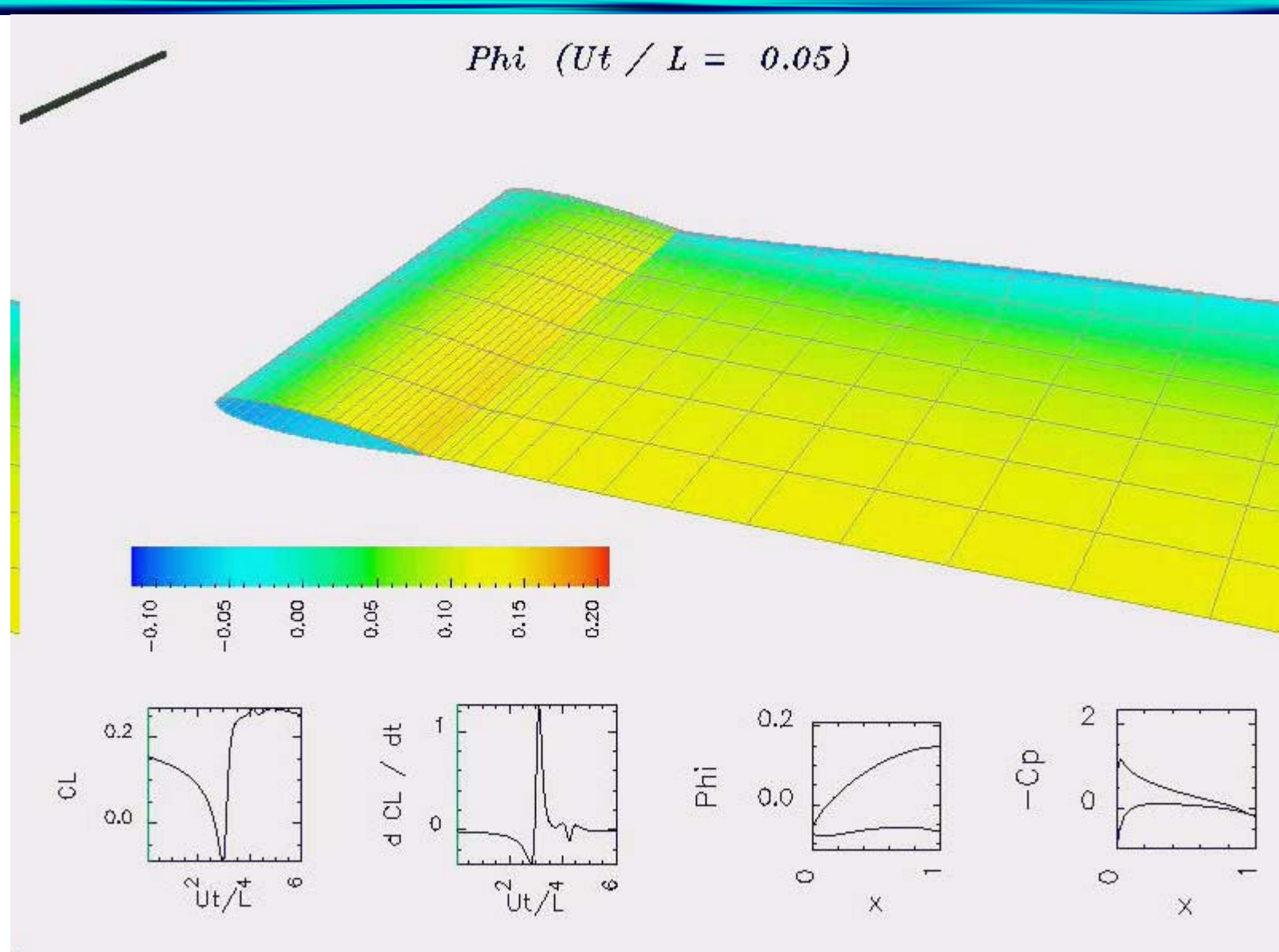


2D propagation
Possio/Atassi

3D propagation
BEM Computation



Blade-Vortex Interaction Problem



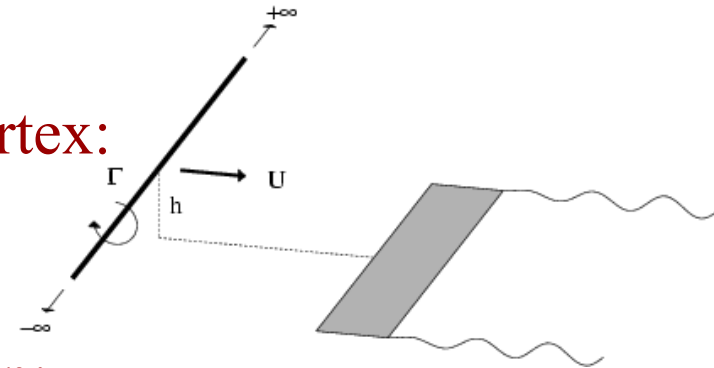


BVI Validation

Analytic frequency response

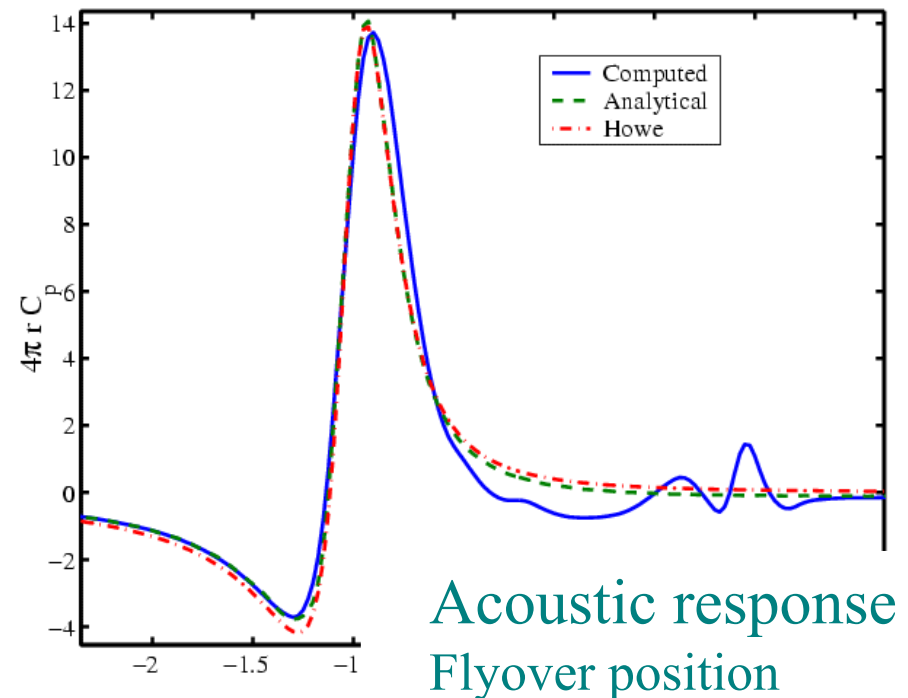
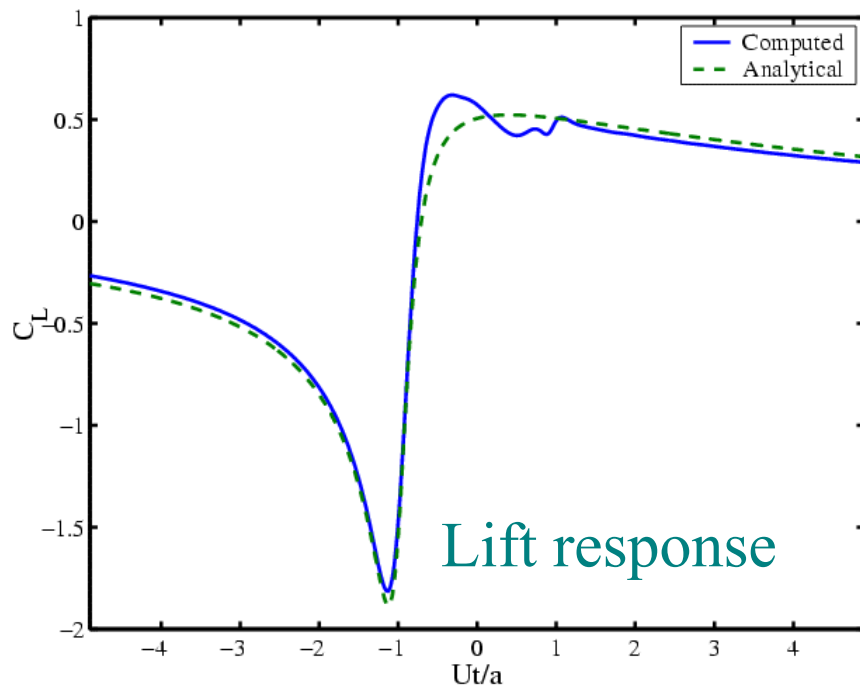
Thin, Flat, unloaded, two-dimensional line vortex:

$$C_l(k) = \frac{i}{2} \Gamma \operatorname{sgn}(k) e^{-i|k|h} S(k)$$

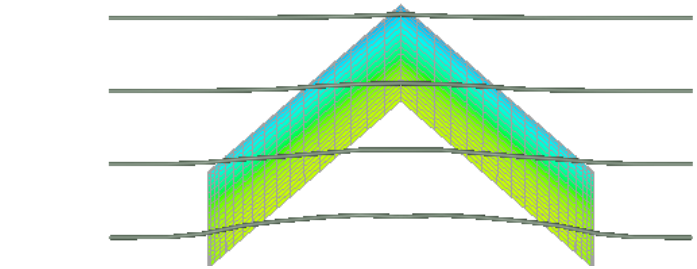


Low Mach number acoustics from Curle's equation:

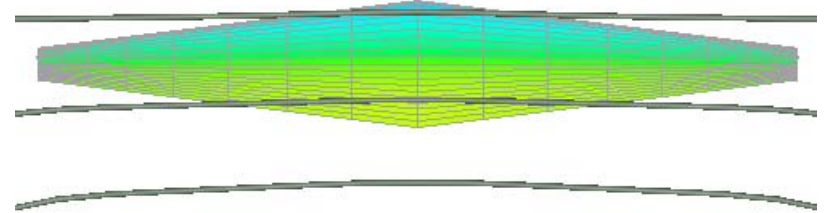
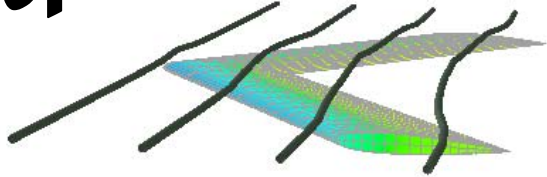
$$C_p(\mathbf{x}, t) \approx \frac{M AR \cos \theta_P}{4\pi r} \left(\frac{\partial C_L}{\partial t} \right)_{t-Mr}$$



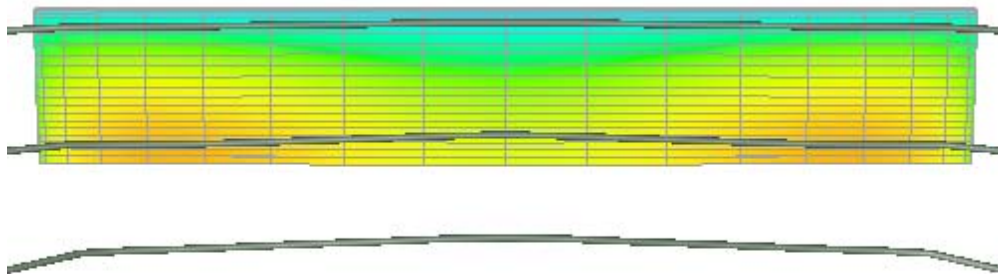
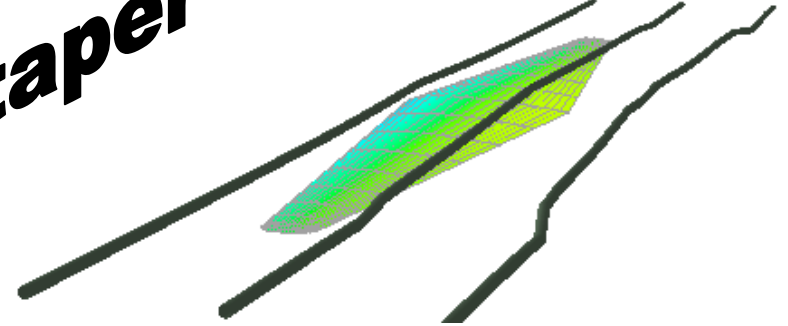
Wing geometry effect



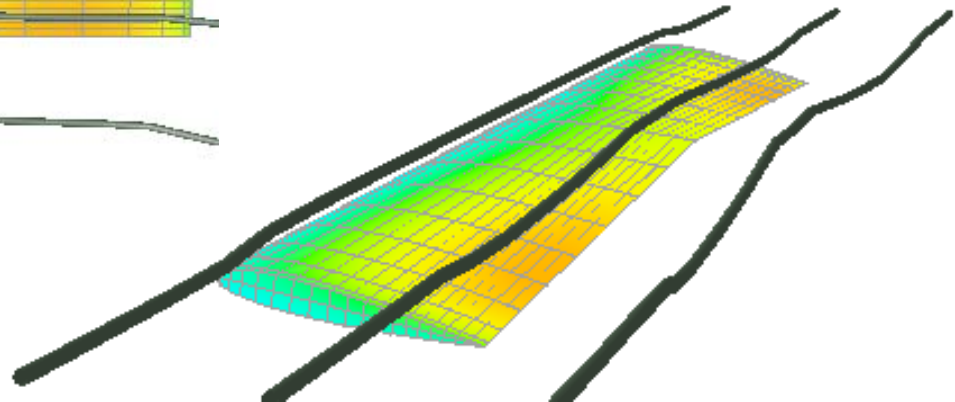
sweep



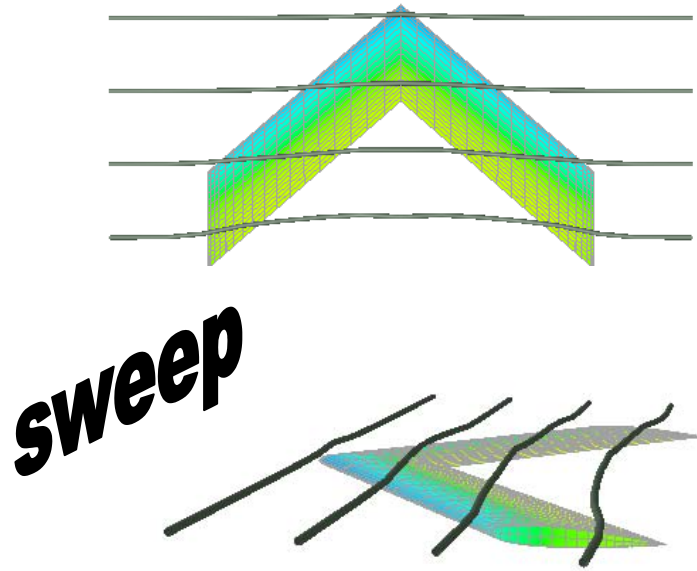
taper



twist

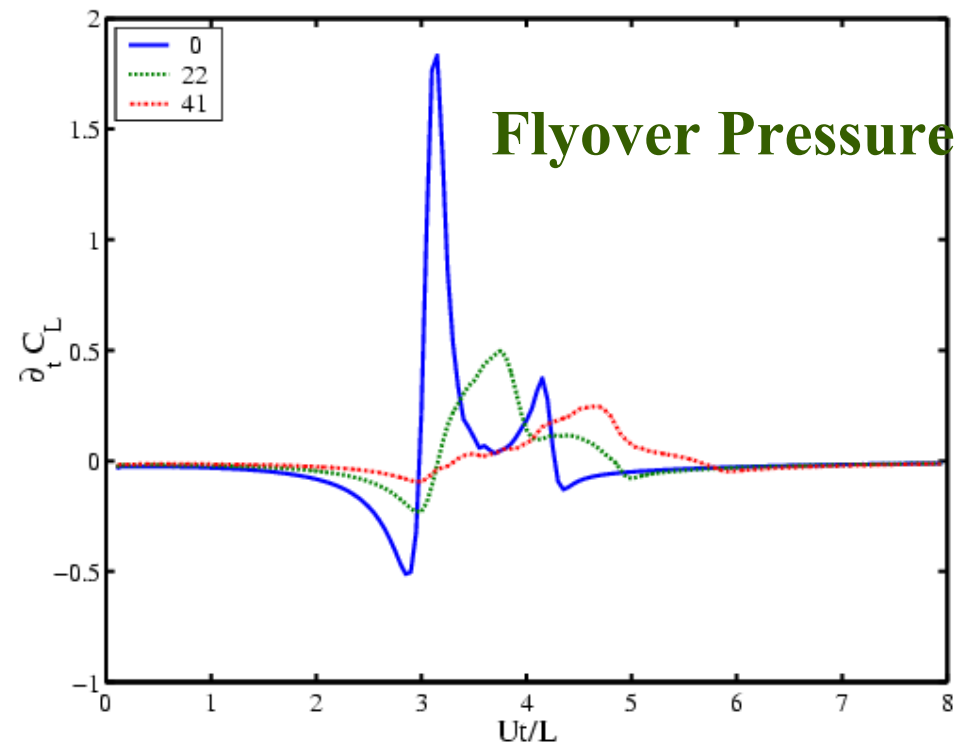
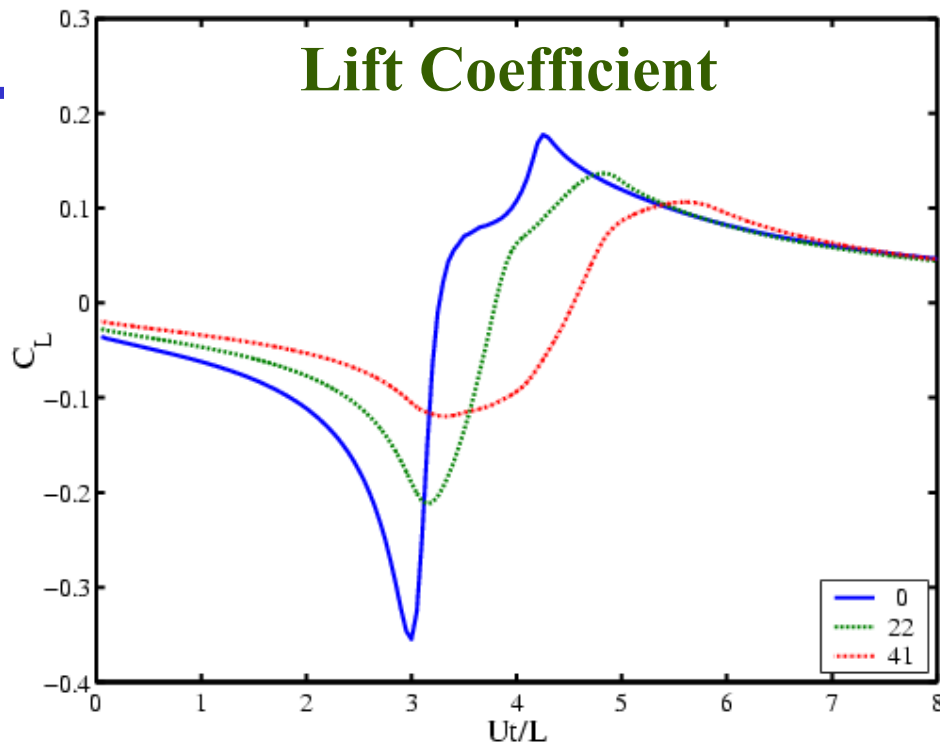


Sweep Effect



Increased sweep

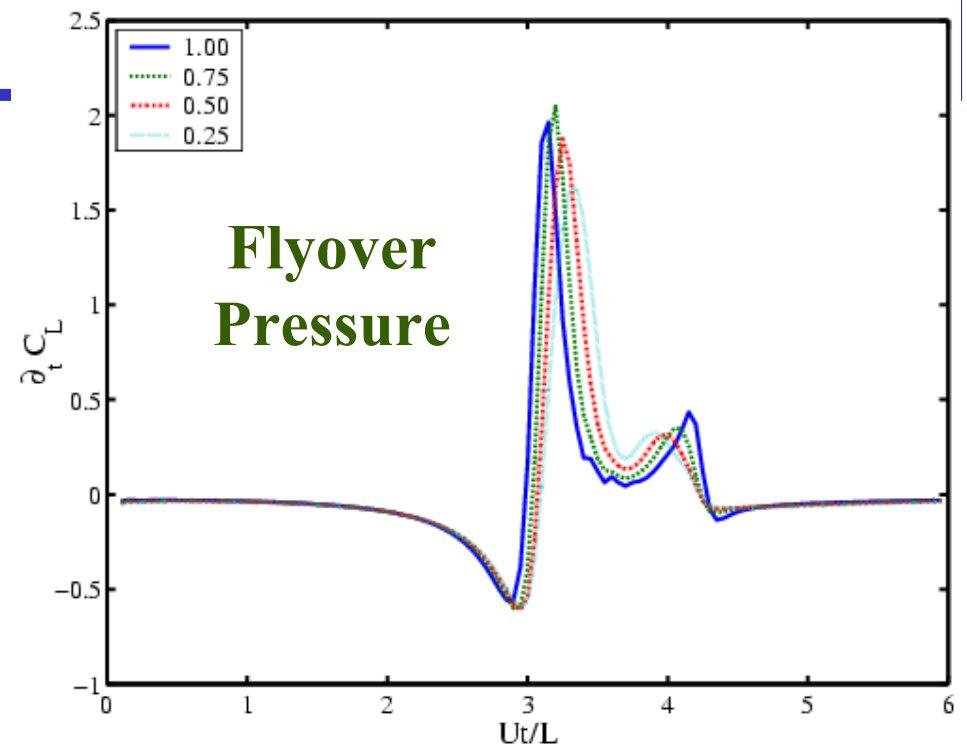
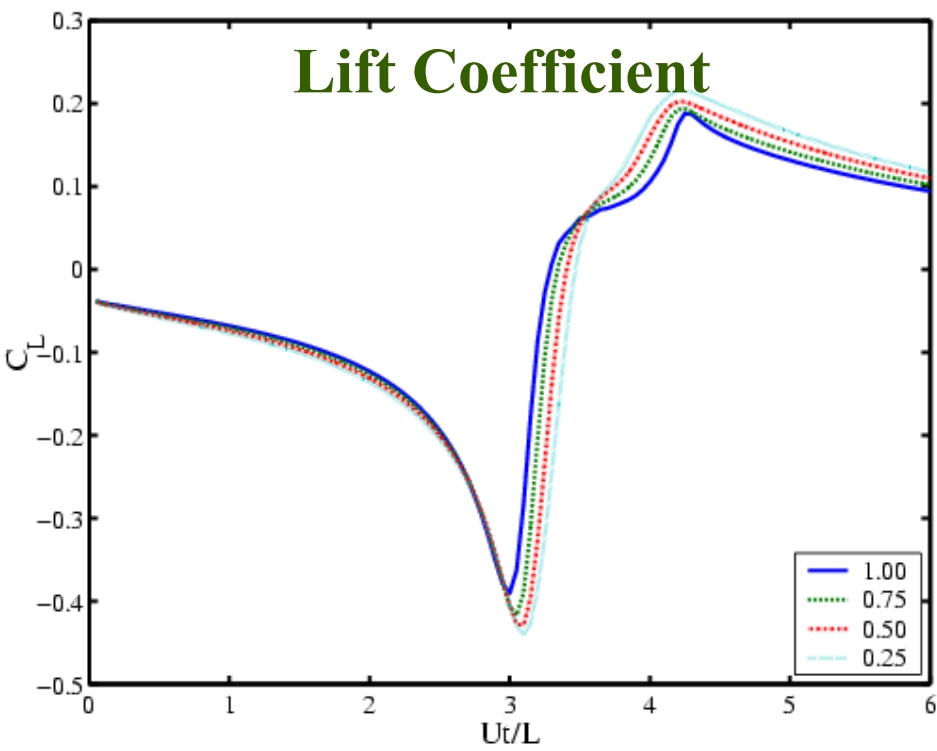
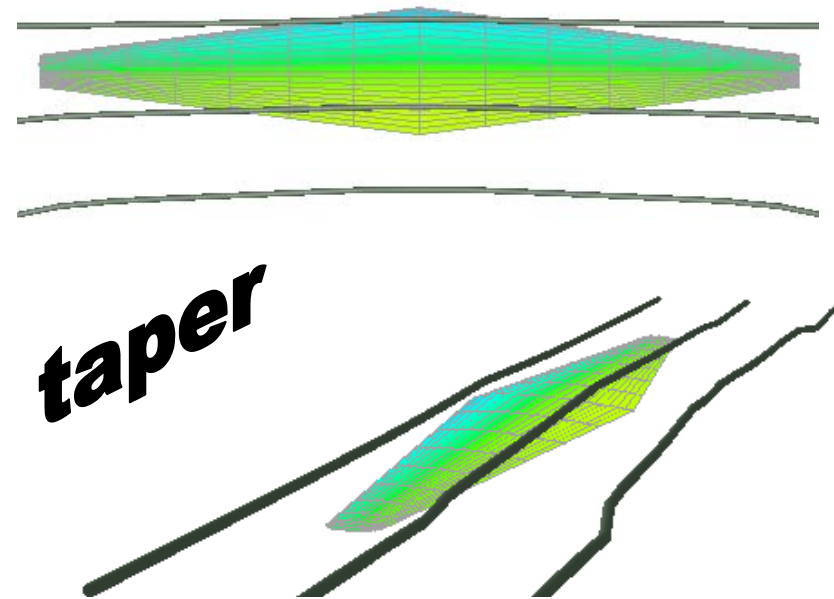
⇒ LE interaction spreads out



Taper Effect

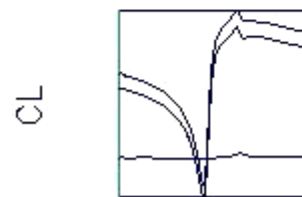
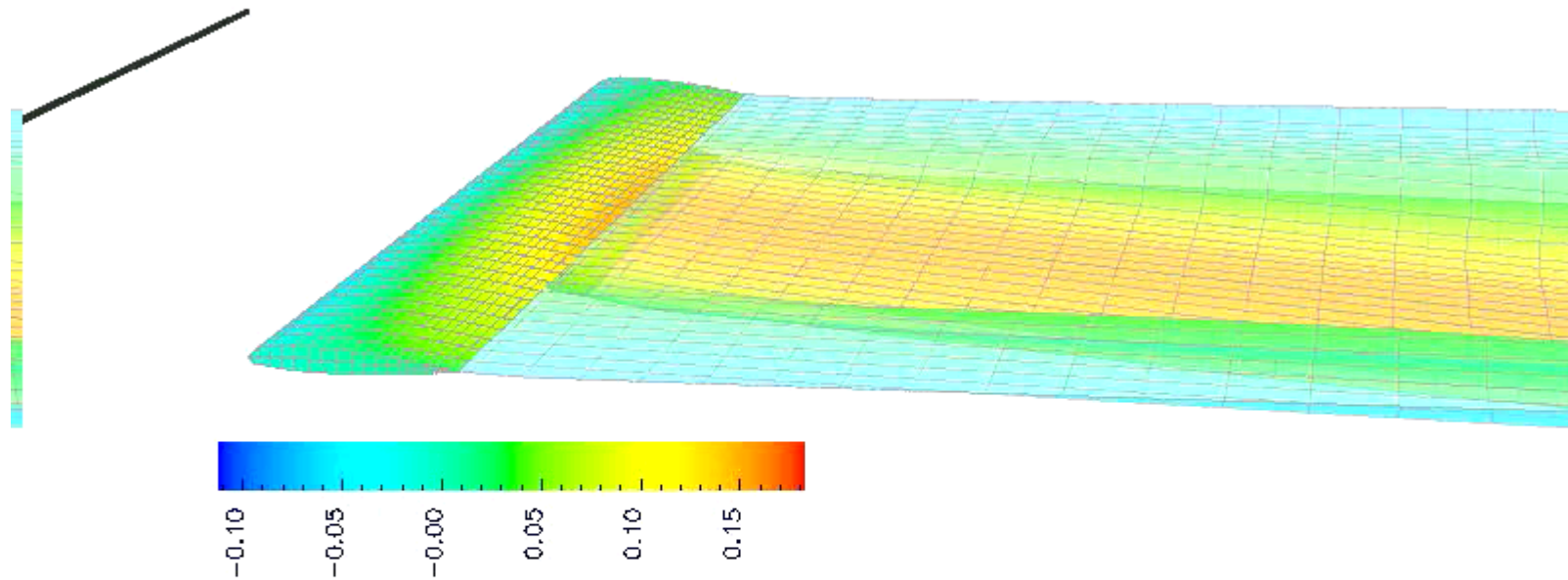
Increased Taper

⇒ slightly decreased acoustics

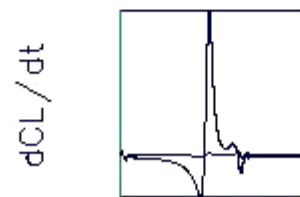


Part span flap

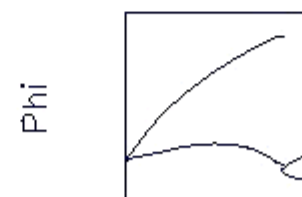
Φ ($Ut / L = 0.05$)



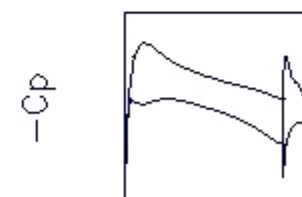
Ut/L



Ut/L



x



x

Conclusions

- **3D BEM validated**
 - Free Wake Evolution
 - **BVI** with Free Vortex Evolution
 - Efficient method for predicting sound from complex wing/blade geometries
- Wing geometry effect
 - Thickness, Camber, Sweep → **decrease** sound
 - Angle of Attack, Flap Deflection → **increase** sound
 - Full-span flap not important sound source
- Flap side-edge; Flap and slat gaps, Slat cove

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