

Buckingham II-Theorem

$a = f(a_1, \dots, a_k, b_1, \dots, b_m)$

↓
dimensional quantity were interested in
parameters with independent dimensions

Construct dimensionless parameters:

$$\Pi = \frac{a}{a_1 \cdots a_k}$$

$$\Pi_1 = \frac{b_1}{a_1^{r_1} \cdots a_k^{r_k}}$$

$$\Pi_2 = \frac{b_2}{a_1^{r_1} \cdots a_k^{r_k}}$$

$$\Pi_m = \frac{b_m}{a_1^{r_1} \cdots a_k^{r_k}}$$

$$\Pi = \Phi(\Pi_1, \Pi_2, \dots, \Pi_m)$$

- sometimes Π has independent dimensions
- sometimes $k=0$
- all parameters/governing parameters are dimensionless

Recall: drag on a sphere

$$D_f = C_D \frac{\rho}{2} V^2 F\left(\frac{R}{V}\right)$$

$$\frac{D_f}{(R/V)^2} = F\left(\frac{R}{V}\right)$$

in general: $k>0$ & $m>0$

Buckingham II-Theorem: The physical relationship between a dimensional quantity and several dimensional parameters can be rewritten as a relationship between a dimensionless parameter and several dimensionless products of the governing parameters. The number of dimensionless products is equal to the number of governing parameters minus the number of independent dimensions.

Essential Dimensionless Products

e.g. $\frac{1}{10} < \Pi_m < 10$

- if Π_m is small or large, assume that it can be neglected

e.g. Brittle fracture

$$D = f(P, K_I, d, \Delta)$$

$$D \sim \left(\frac{P}{K_I}\right)^{1/2} \Phi\left(\frac{d}{\Pi_1}, \frac{\Delta}{\Pi_2}, \frac{P}{\Pi_3}\right)$$

$$\Pi_1 \ll 1 \quad \& \quad \Pi_2 \gg 1$$

more formally:
- Π_m that is small or large can be neglected
- if $\Phi(\dots)$ has a finite, non-zero limit as
 $\Pi_m \rightarrow 0$ or $\Pi_m \rightarrow \infty$

Complete Similarity or Similarity of the First Kind

Incomplete Similarity or Similarity of the Second Kind

- if $\Pi_m \rightarrow 0$ or $\Pi_m \rightarrow \infty$ the function $\Phi(\dots)$ does not have a finite and non-zero limit
- but can remain essential as either how small or large its corresponding dimensionless parameter becomes
- if $\Phi(\dots)$ has a power-like asymptotic representation, then you can rewrite it as

$$\Phi = \Pi_m^\alpha \Phi_1(\Pi_1, \dots, \Pi_{m-1}) + O(\Pi_m^\alpha)$$

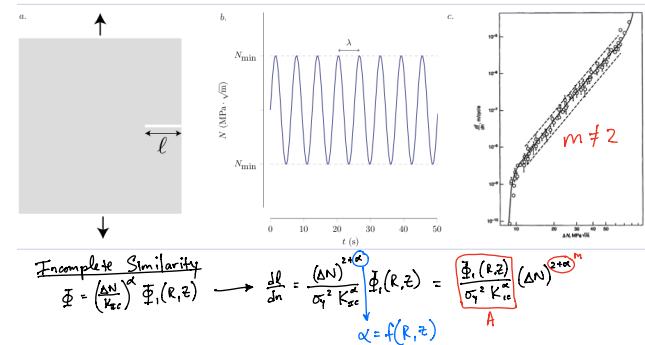
small compared with first term

$$\Pi^* = \Phi_1(\Pi_1, \dots, \Pi_{m-1})$$

$$\frac{\Pi}{\Pi_m} = \frac{a}{a_1^{r_1} \cdots a_k^{r_k} b_m} \rightarrow \text{still applies}$$

may depend on the dimensionless products
 $\propto \& \Pi^*$
cannot be determined by dimensional analysis alone

Fatigue: Incomplete Similarity



$$\text{Incomplete Similarity} \rightarrow \frac{da}{dt} = \frac{(\Delta N)^{2+\alpha}}{\sigma_I^2 K_{Ic}^2} \Phi_1(R, z) = \frac{\Phi_1(R, z)}{\sigma_I^2 K_{Ic}^2} (\Delta N)^{2+\alpha}$$

$\alpha = f(R, z)$

$$\frac{da}{dt} = A(\Delta N)^m$$

material properties?
geometry or specimen size?
yield stress

$$\frac{da}{dt} = f(\Delta N, \frac{N_{max}}{N_{min}}, f, t, h, \sigma_I, K_{Ic})$$

stress intensity factor

$$\frac{da}{dt} = \left(\frac{\Delta N}{\sigma_I}\right)^2 \Phi_1\left(\frac{\Delta N}{K_{Ic}}, R, \frac{\sigma_I}{K_{Ic}}, f\right)$$

small

neglect

$$\frac{da}{dt} = \left(\frac{\Delta N}{\sigma_I}\right)^2 \Phi_1(R, z) = \frac{\Phi_1(R, z)}{\sigma_I^2} (\Delta N)^2$$

\cancel{A} $m \neq 2$